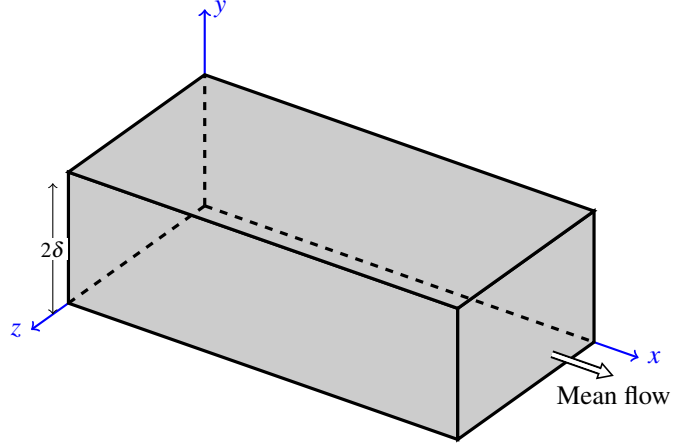


Definitions

- U_1 , streamwise mean velocity ($U_2 \equiv 0$; $U_3 \approx 0$)
- u_1, u_2, u_3 , are the fluctuating velocities along x, y, z , coordinates respectively
- ν , kinematic viscosity
- Homogeneous along x and z direction, i.e., $\partial_x(\cdot) = \partial_z(\cdot) = 0$



Statistical moments and their budgets

The second-, third- and fourth-order moments of the Navier-Stokes equations for the case of parallel flow are given in Equations (1), (2) and (3), respectively. The terms written on the right-hand-side balance the total derivative. For parallel-flows the spatial gradient in the convective term is zero. Furthermore, with a constant streamwise pressure gradient, the temporal derivative is zero. Hence in the unstrained fully-developed channel flow, $D_t = 0$. Due to straining the material derivative is $\mathcal{D}_t = \partial_t \neq 0$. The applied strain causes the moments to evolve in time, analogous to spatial development of an adverse pressure gradient boundary layer. In otherwords, spatial derivative is replaced by a time derivative.

$$\partial_t \overline{u_i u_j} = \mathcal{P}_{ij}^S + \mathcal{P}_{ij}^A + \mathcal{T}_{ij} + \Pi_{ij} + \varepsilon_{ij} + \mathcal{D}_{ij} \quad (1)$$

where

$$\begin{aligned} \mathcal{P}_{ij}^S &= -\overline{u_i u_2} \partial_2 U_j - \overline{u_j u_2} \partial_2 U_i \\ \mathcal{P}_{ij}^A &= -\overline{u_i u_k} A_{jk} - \overline{u_j u_k} A_{ik} \\ \mathcal{T}_{ij} &= -\partial_2 \overline{u_2 u_i u_j} \\ \Pi_{ij} &= -(1/\rho)(\overline{u_j \partial_i p} + \overline{u_i \partial_j p}) \\ \varepsilon_{ij} &= -2\nu \overline{\partial_k u_i \partial_k u_j} \\ \mathcal{D}_{ij} &= \nu \partial_2^2 \overline{u_i u_j} \end{aligned}$$

$$\partial_t \overline{u_i u_j u_l} = \mathcal{P}_{ijl}^S + \mathcal{P}_{ijl}^A + \mathcal{P}_{ijl}^T + \mathcal{T}_{ijl} + \Pi_{ijl} + \varepsilon_{ijl} + \mathcal{D}_{ijl} \quad (2)$$

where

$$\begin{aligned} \mathcal{P}_{ijl}^S &= -\overline{u_i u_j u_2} \partial_2 U_l - \overline{u_j u_l u_2} \partial_2 U_i - \overline{u_l u_i u_2} \partial_2 U_j \\ \mathcal{P}_{ijl}^A &= -\overline{u_i u_j u_k} A_{lk} - \overline{u_j u_l u_k} A_{ik} - \overline{u_l u_i u_k} A_{jk} \\ \mathcal{P}_{ijl}^T &= \overline{u_i u_j} \partial_2 \overline{u_2 u_l} + \overline{u_j u_l} \partial_2 \overline{u_2 u_i} + \overline{u_l u_i} \partial_2 \overline{u_2 u_j} \\ \mathcal{T}_{ijl} &= -\partial_2 \overline{u_2 u_i u_j u_l} \\ \Pi_{ijl} &= -(1/\rho)(\overline{u_i u_j \partial_l p} + \overline{u_j u_l \partial_i p} + \overline{u_l u_i \partial_j p}) \\ \varepsilon_{ijl} &= -2\nu(\overline{u_i \partial_k u_j \partial_k u_l} + \overline{u_j \partial_k u_i \partial_k u_l} + \overline{u_l \partial_k u_i \partial_k u_j}) \\ \mathcal{D}_{ijl} &= \nu \partial_2^2 \overline{u_i u_j u_l} \end{aligned}$$

$$\partial_t \overline{u_i u_j u_l u_m} = \mathcal{P}_{ijlm}^S + \mathcal{P}_{ijlm}^A + \mathcal{P}_{ijlm}^T + \mathcal{T}_{ijlm} + \Pi_{ijlm} + \varepsilon_{ijlm} + \mathcal{D}_{ijlm} \quad (3)$$

where

$$\begin{aligned} \mathcal{P}_{ijlm}^S &= -\overline{u_i u_j u_l u_m} \partial_2 U_m - \overline{u_j u_l u_m u_i} \partial_2 U_i - \overline{u_l u_m u_i u_j} \partial_2 U_j - \overline{u_m u_i u_j u_l} \partial_2 U_l \\ \mathcal{P}_{ijlm}^A &= -\overline{u_i u_j u_l u_k} A_{mk} - \overline{u_j u_l u_m u_k} A_{ik} - \overline{u_l u_m u_i u_k} A_{jk} - \overline{u_m u_i u_j u_k} A_{lk} \\ \mathcal{P}_{ijlm}^T &= \overline{u_i u_j u_l \partial_2 u_m} + \overline{u_j u_l u_m \partial_2 u_i} + \overline{u_l u_m u_i \partial_2 u_j} + \overline{u_m u_i u_j \partial_2 u_l} \\ \mathcal{T}_{ijlm} &= -\partial_2 \overline{u_i u_j u_l u_m} \\ \Pi_{ijlm} &= -(1/\rho) (\overline{u_i u_j u_l \partial_m p} + \overline{u_j u_l u_m \partial_i p} + \overline{u_l u_m u_i \partial_j p} + \overline{u_m u_i u_j \partial_l p}) \\ \varepsilon_{ijlm} &= -2\nu (\overline{u_i u_j \partial_k u_l \partial_k u_m} + \overline{u_i u_l \partial_k u_j \partial_k u_m} + \overline{u_j u_l \partial_k u_i \partial_k u_m} \\ &\quad + \overline{u_j u_m \partial_k u_l \partial_k u_i} + \overline{u_l u_m \partial_k u_j \partial_k u_i} + \overline{u_m u_i \partial_k u_l \partial_k u_j}) \\ \mathcal{D}_{ijlm} &= \nu \partial_2^2 \overline{u_i u_j u_l} \end{aligned}$$

In equation 1-3, budgets on the right hand side are termed as ‘production’ due to shear (\mathcal{P}^S), ‘production’ due to Reynolds stress (\mathcal{P}^T), turbulent transport (\mathcal{T}), velocity-pressure gradient correlation (Π), ‘dissipation’ (ε) and viscous diffusion (\mathcal{D}). The applied strain produces source terms in all the moment equations, which is called ‘production’ due to applied strain (\mathcal{P}_{ij}^A). The terminologies used to describe the budget terms are inherited from second-moment closure, and do not necessarily represent physical behavior (e.g., ‘production’ can be negative and ‘dissipation’ can be positive).

The velocity pressure gradient term is decomposed as $\Pi = \psi + \phi$, where ψ is pressure transport term and ϕ the pressure-strain term. Expressions of the decomposed terms in the second-, third- and fourth-order moment are given below.

$$\psi_{ij} = \frac{-1}{\rho} \left(\partial_2 \overline{p u_j} \delta_{2i} + \partial_2 \overline{p u_i} \delta_{2j} \right) \quad (4)$$

$$\phi_{ij} = \frac{1}{\rho} \left(\overline{p \partial_i u_j} + \overline{p \partial_j u_i} \right) \quad (5)$$

$$\psi_{ijl} = \frac{-1}{\rho} \left(\partial_2 \overline{p u_i u_j} \delta_{2l} + \partial_2 \overline{p u_j u_l} \delta_{2i} + \partial_2 \overline{p u_l u_i} \delta_{2j} \right) \quad (6)$$

$$\phi_{ijl} = \frac{1}{\rho} \left(\overline{p \partial_l u_i u_j} + \overline{p \partial_i u_j u_l} + \overline{p \partial_j u_l u_i} \right) \quad (7)$$

$$\psi_{ijlm} = \frac{-1}{\rho} \left(\partial_2 \overline{p u_i u_j u_l} \delta_{2m} + \partial_2 \overline{p u_j u_l u_m} \delta_{2i} + \partial_2 \overline{p u_l u_m u_i} \delta_{2j} + \partial_2 \overline{p u_m u_i u_j} \delta_{2l} \right) \quad (8)$$

$$\phi_{ijlm} = \frac{1}{\rho} \left(\overline{p \partial_m u_i u_j u_l} + \overline{p \partial_i u_j u_l u_m} + \overline{p \partial_j u_l u_m u_i} + \overline{p \partial_l u_m u_i u_j} \right) \quad (9)$$