



Overflow Juncture Flow Computations Compared with Experimental Data

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NASA's Transformational Tools and Technologies Project (T^3) is supporting a substantial effort to investigate the formation and origin of separation bubbles found on wing-body juncture zones: the Juncture Flow experiment. The first phase of the Juncture Flow experiment, performed in NASA Langley's 14- by 22-Foot Subsonic Tunnel, has been completed. This paper documents the CFD analysis done in conjunction with the experiment. Comparisons between CFD simulations and wind tunnel experimental results will be shown. Oil flow results, surface pressure cuts, velocity profiles, and Reynolds stress profiles will be compared. Preliminary results analyzing the effect of grid resolution, wind tunnel walls, and turbulence models on the above data will be presented. The results are not meant to be a validation study, but more as an evaluation of the current status of Reynolds averaged Navier Stokes (RANS) CFD simulations.

I. Introduction

Juncture flows are very difficult to predict, even with the current state-of-the-art CFD methods. In the AIAA drag prediction workshop 3 (DPW-3), which used the DLR-F6 wing-body, participants predicted a very wide range of side-of-body separations.^{1,2} The same issue arose for the Common Research Model (CRM) in DPW-4 and DPW-5.³ The introduction of the quadratic constitutive relation (QCR) by Spalart [4] did make the predicted separation bubble sizes over various CFD codes more homogeneous, but the solutions are still over-predicting bubble size when compared to experimental results.

There have been multiple experiments dedicated to juncture flow regions, most notable Simpson [5] and Gand et al. [6] with the ONERA group, but very few were able to obtain measurements in the trailing-edge corner separation, on a swept wing configuration. Simpson's work focused more on the leading edge horseshoe vortex, while ONERA's experiment was an unswept wall-mounted wing.

NASA, through its Transformational Tools and Technologies Project (T^3) under Transformative Aeronautics Concepts Program (TACP), is supporting a substantial effort, the Juncture Flow (JF) experiment, to investigate the formation and origin of separation bubbles found on wing-body juncture zones. The experiment is intended to be primarily for the purpose of CFD validation and turbulence model development for wing-juncture trailing edge separation onset and progression. The committee members decided upon a sting-mounted swept-wing and fuselage model, with a Laser Doppler velocimetry (LDV) system inside the fuselage (as opposed to the traditional LDV system mounted behind the wind tunnel walls). The goal was to observe the onset and growth of the separation bubble in aft juncture flow region of a realistic wing-body configuration. Placing the LDV system inside the fuselage provides a way to measure the leading-edge and trailing-edge juncture regions. The Juncture Flow Model (JFM) is a reduced scale model, i.e. 8%, based on the full scale CRM.

A campaign of risk reduction experiments, and accompanying CFD simulations, including:

1. Fluid Mechanics Lab (FML) Test Cell 2 at NASA Ames Research Center 3% semispan model⁷
2. Virginia Tech Stability Tunnel 2.5% model⁸
3. NASA Langley 14-by-22 Ft. Subsonic Wind Tunnel 6% model⁹

helped finalize the experiment design and maximize the value of the data obtained in the final tests. The JF team settled on two different interchangeable wing configurations, including a wing based on a DLR-F6 wing and a NACA

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based wing, for the final test. Only the former wing was tested in the wind tunnel campaign performed in late 2017 and early 2019.

Experimental data and Overflow CFD data will be presented. Data including oil flow results, surface pressure cuts, Reynolds stress profiles, and velocity profiles will be compared. Preliminary results pertaining to CFD sensitivity to parameters including grid resolutions, turbulence models, and wall effects will be explored. Further details on the experimental setup and results can be found in a companion paper by Kegerise et al. [10], and further CFD comparisons can be found in Rumsey et al. [11].

This paper is not meant to serve as a validation of the CFD solvers, but more so as an evaluation of the current state of CFD simulations. The experiment was designed using CFD analysis, and now that experimental data is available, we would like to assess how well the CFD simulations performed.

II. 14-by-22 Foot Subsonic Wind Tunnel JFM Experiment

The JFM experiment was performed in the 14-by-22 Ft. Subsonic Tunnel (14x22), and the full results can be found in Kegerise et al. [10]. A very brief description of the relevant experimental setup will be presented below. The subsequent subsections will discuss the 14x22 wind tunnel and the Juncture Flow Model.

A. 14-by-22 Ft. Subsonic Wind Tunnel

The experiment was performed in the Langley 14-by-22 Ft. Subsonic Tunnel (14x22), which is a closed-circuit, atmospheric-pressure wind tunnel. This test was made in the closed test section mode, which results in a 14.5 ft high and 21.75 ft wide test section. Figure 1a shows the full circuit of the 14x22 with the high speed leg outlined in blue, and 1b describes the sections of the high speed leg.

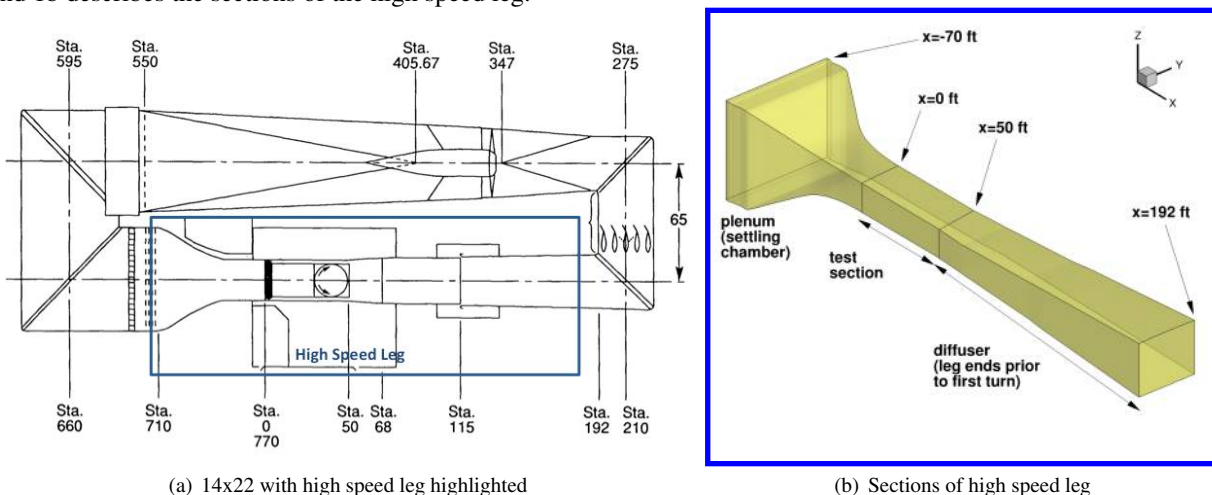


Figure 1. 14x22 Wind Tunnel, High Speed Leg

Further details about the tunnel can be found in Gentry et al. [12]. The flow condition of primary interest for this experiment was $Re_c = 2.4$ million.

B. Juncture Flow Model

The Juncture Flow Model is a large aluminum model consisting of a fuselage and a number of interchangeable wing candidates. The model wing span was nominally 3397.250 mm, fuselage length was 4839.233 mm, and crank chord (the chord at the y-station with trailing edge break) was 557.17 mm. The fuselage nose is at $x = 0\text{ mm}$, the x-axis was aligned with the fuselage centerline, the y-axis ran starboard, and the z-axis was up. The fuselage side wall is planar over much of the body (to make it easier to install windows for the laser-based measurement systems), at $y = 236.1\text{ mm}$. The F6 wing leading edge horn is located near $x = 1925.0\text{ mm}$ at the fuselage, while the F6 wing root trailing edge is located at $x = 2961.9\text{ mm}$. The fuselage housed two separate LDV systems, mounted on a traverse system. The port side of the fuselage has a set of windows upstream of the wing leading edge, as well as on the trailing edge. The wings are designed to have removable leading edge horns. This paper will focus on the model with the

leading edge horn installed, which has the largest experimental dataset. Further information of the experiment setup can be found in Kegerise et al. [10]. Figure 2 details the parts on the JFM.

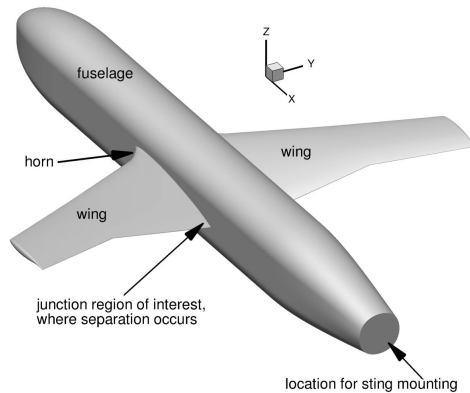


Figure 2. Juncture Flow Model Parts.

III. Computational Fluid Dynamics, Overflow

CFD solutions are performed with Overflow. Simulations are run in air, first, and then with the wind tunnel walls, to assess the wall effects. The subsequent sections will cover how the Overflow simulations are set up.

A. Overflow Setup

A series of overset grids were created for the Juncture Flow Model. There is a commonality between the grids used in all of the CFD simulations. The grids are built using Chimera Grid Tools.¹³ The full span JFM configuration consists of a fuselage, and two wings. The fuselage is built from 4 zones, two of which span the length of the fuselage, and two cap grids covering the nose and rear of the fuselage. The wing grids for all the various configurations share a common 6 zone topology. The wing grids consist of two collar grids covering the wing-fuselage junction, two grids spanning the wing, and two wing tip cap grids. Each pair of grids have overlap along the chord, making effectively a front and rear zone. All the surface grids are projected back to the reference CAD geometry using Pointwise¹⁴ to ensure a smooth surface geometry.

For the free air grids, a series of grids with increasing grid resolution are built. Four grid topologies, including a coarse, medium, fine, and extra-fine grid, were constructed. Figure 3 shows the grid density on the surface of the port wing and fuselage, as well as a zoomed in view of the root-trailing edge region. The overall vehicle includes 16 grid zones, and Table 1 details the various configurations looked at in this study, and the grid metrics for each configuration. The near body grid point counts include just the volume grids for the JFM, excluding the support hardware, and applicable wind tunnel or off-body Cartesian grids.

Table 1. Overflow Grid Summary

Configuration	Max Stretching Ratio	Near Body Grid Points	Total Grid Points
Air Coarse	1.20	19,370,462	21,374,660
Air Medium	1.15	47,580,599	49,726,586
Air Fine	1.10	163,552,251	165,714,572
Air Extra Fine	1.08	382,086,347	398,391,568
Wind Tunnel Medium	1.15	47,580,599	92,582,251
Wind Tunnel Fine	1.10	163,552,251	325,462,526

For all the free air cases, the JFM grids are embedded in Overflow's off-body Cartesian grid system. Domain

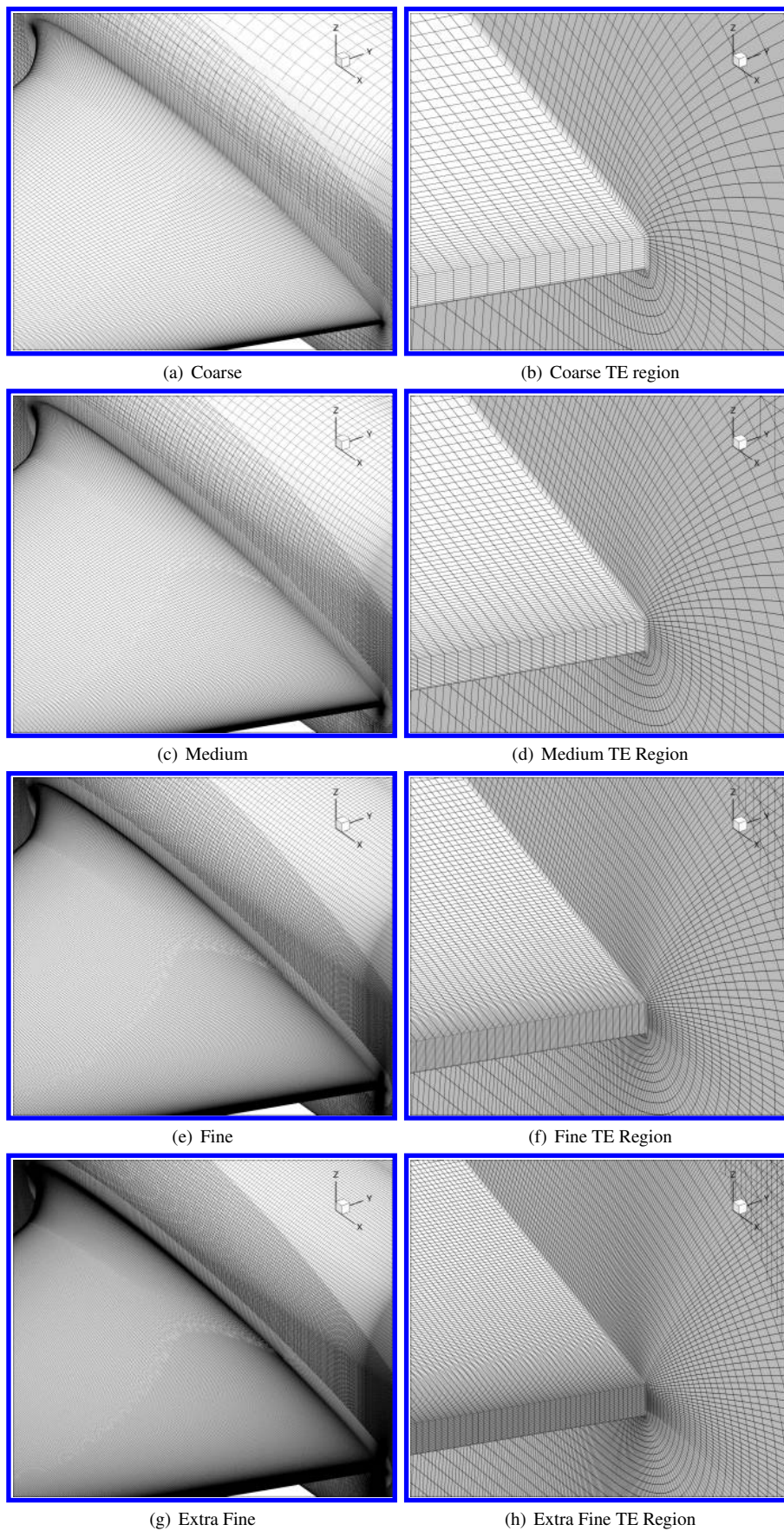


Figure 3. JFM Surface Grid Resolutions.

connectivity is performed using Overflow's object x-rays.¹⁵ The far-field domain is set to be 100 chord lengths away. The free air simulations are run at Mach number $M_\infty = 0.189$ at $T = 519.912$ Rankine, with a Reynolds number of 2.4 million based on the yehudi break chord. The free air simulations are run at an uncorrected angle of attack of -2.5° and 5.0° . Theoretically, there should be an angle of attack correction to account for the wall effects, but this data was unavailable at the time of the test.

All of the Overflow cases are run with Overflow 2.2N. The 3rd-order Roe upwind scheme¹⁶ is used for the convective fluxes, and the implicit solve was done using ARC3D Beam-Warming scalar pentadiagonal scheme and low-Mach preconditioning.¹⁷ The Spalart-Allmaras turbulence model with the rotational correction (RC) and QCR2013¹⁸ is used for most of the cases. All the cases were run fully turbulent. Additional cases looking at turbulence model effects on the juncture flow region will be explored later in Section IV.C. The effect of not using QCR, as well as using the SST turbulence model with the rotational correction and QCR will be compared.^{19,20} In short, solutions with three turbulence models:

1. SA-Noft2-RC-QCR2013 (SARC-QCR)¹⁸
2. SA-Noft2-RC (SARC)²¹
3. SST-RC-QCR2013 (SSTRC-QCR)²⁰

will be presented. The CFD free air (CFD air) results are computed using 420 Intel Broadwell cores, and utilized approximately 12 hours of walltime.

For the wind tunnel grids, wall grids are built from the as-built laser scanned CAD as specified in Nayani et al. [22]. Fifteen zones modeled the high-speed leg of the 14x22. The tunnel is split into five sections streamwise: plenum, test section, diffuser part 1, diffuser part 2, and extended diffuser. Each section was comprised of two viscous wall grids, and one core grid. The average grid spacing is varied to produce a medium (0.5 ft., 152.4 mm), and fine (0.25 ft., 76.2 mm) grid. Minimum spacing at the walls of the test section is less than 0.00001 ft. (0.003048mm) on all grids. The straight section of the inlet, prior to the contraction, is run with inviscid walls. The diffuser grids gradually coarsened downstream. A diffuser extension of 100 ft. (30,480 mm) streamwise is incorporated, and the extended diffuser walls also use an inviscid boundary condition. Figure 4 shows the wind tunnel volume grid with the extended diffuser, and an overall view of the 14x22 with the JFM installed. Utilizing inviscid spans of the tunnel help increase the code stability at the boundary conditions, and help accelerate the convergence of the CFD code. The details and benefits of using this method can be found in by Lee et al. [23]. Domain connectivity and hole cutting was performed using Overflow's object x-rays as well.¹⁵

The JFM installation location for both $\alpha = 5.0^\circ$ and $\alpha = -2.5^\circ$ cases was based on CAD. Different geometries were necessary for the two angles of attack, as the mast on the support did change to place the model in the center of the tunnel. Figure 5 shows a zoomed in region of the test section with the JFM installed at both angles of attack. There is a slight variation of the angle of attack ($\pm 0.05^\circ$) throughout the test that the CFD does not account for. For the wind tunnel results shown below, the free air medium and fine grids were embedded directly into the wind tunnel configuration for consistency between and free air and tunnel calculations.

The wind tunnel with the JFM installed (at their respective angles of attack) were translated and rotated to match the same coordinate system as the free air grid system (body coordinate system), to greatly simplify the post processing. In doing this, all the flow quantities, velocities, etc. from a post processing standpoint, were already in the JFM body coordinate system as opposed to the tunnel coordinate system. This eliminates the need to transform the flow data to the body coordinate system when post processing the data.

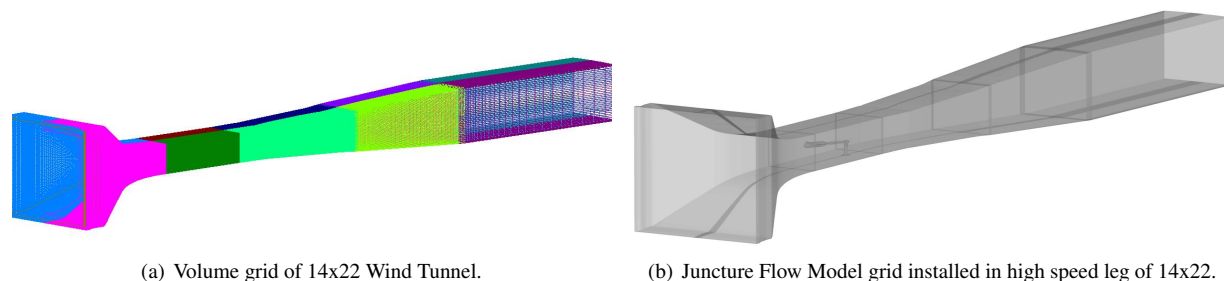
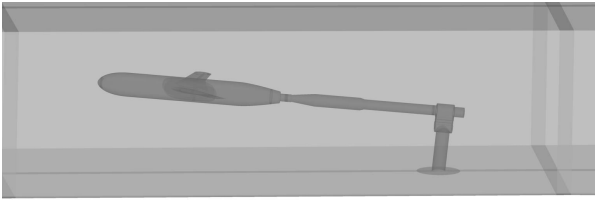
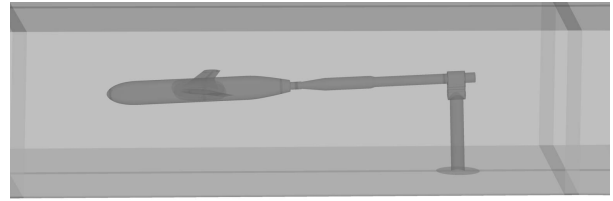


Figure 4. 14x22 Foot Subsonic Wind Tunnel, high speed leg with extended diffuser.

In the 14x22 wind tunnel, the Reynolds number is held constant at 2.4 million ($\pm 0.3\%$) based on the crank cord. Throughout the testing, the atmospheric conditions did change, resulting in a spread of Mach numbers ranging from 0.175 to 0.205, temperatures ranging from 495 to 554.4 Rankine ($275 - 308^\circ K$), and dynamic pressures ranging



(a) Junction Flow Model in 14x22 at $\alpha = 5.0^\circ$.



(b) Junction Flow Model in 14x22 at $\alpha = -2.5^\circ$.

Figure 5. Junction Flow Model as installed in the 14x22 Foot Subsonic Wind Tunnel.

from 2107 to 2921 Pa. Median values were chosen for the CFD air runs, and they correspond to $M_\infty = 0.189$, and $T = 519.912$ Rankine.

The wind tunnel also is modeled using the same chosen $M_\infty = 0.189$, a reference temperature of $T = 519.912$ Rankine ($T = 288.84$ K), and a Reynolds number of 2.4 Million based on the yehudi break chord. Stagnation temperature and stagnation pressure based on a reference condition of $M_\infty = 0.189$ are imposed at the inlet boundary, and a back pressure ratio is specified at the tunnel exit. A combination of the static and stagnation pressure measurements are used to calculate the tunnel speed, and the back pressure was iterated until the wind tunnel reached the desired conditions. More on this method of simulating the wind tunnel can be found in Lee et al. [23].

The CFD wind tunnel (CFD wind tunnel) simulations used 800 Intel Skylake Cores, for anywhere between 60 to 120 hours of walltime. The wind tunnel simulations take a lot longer to run, due to the need to iterate the back pressure to get the tunnel conditions to match. Using a proportional–integral–derivative controller (PID)²⁴ to drive the correct back pressure did help, but still requires a considerable run time. Table 1 outlines the JFM number of grid points and total number of grid points for each of the CFD wind tunnel cases.

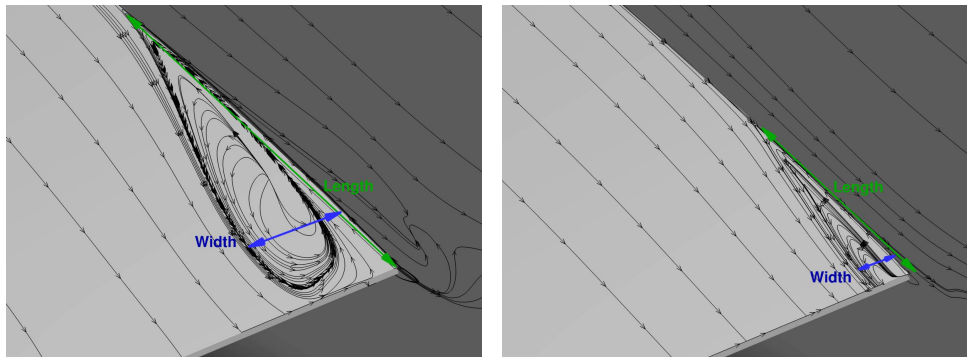
IV. Results

The Overflow computational simulations will be compared with experimental results.¹⁰ Side-of-body bubble separation separation widths, pressure coefficient (C_P), velocity and Reynolds stress plots and profiles will be presented. CFD solutions, in air and with wind tunnel wall, with varying grid resolutions will be presented. Variations in turbulence models (in air) will also be shown. The larger number of results presented here are free air computations which is the typical mode of operation for CFD studies. Free air computations converge faster than the wind tunnel calculations, due in part to the need to calibrate each run in the wind tunnel for a consistent Mach number incoming to the model, and also due to the smaller grid requirements. As will be shown below, in most cases the free air results and wind tunnel results are consistent, sometimes for specific quantities, (e.g. pressure distributions away from the juncture flow region and wing tip), and even when not comparable in certain regions, the trends are consistent.

Figure 6 shows a representative side of body separation width and length for $\alpha = 5.0^\circ$ and $\alpha = -2.5^\circ$, and indicate that data was taken from the CFD computation (surface streamlines) by finding a dividing particle trace line from the separation inception and using that to define length and maximum width. Note that there is a fair amount of arbitrariness to the extracted values. Velocity profiles and Reynolds stresses from both the LDV data and CFD extractions will be shown. Experimental data will always be plotted in black, with uncertainties representing a 95% confidence interval (2σ) when available.

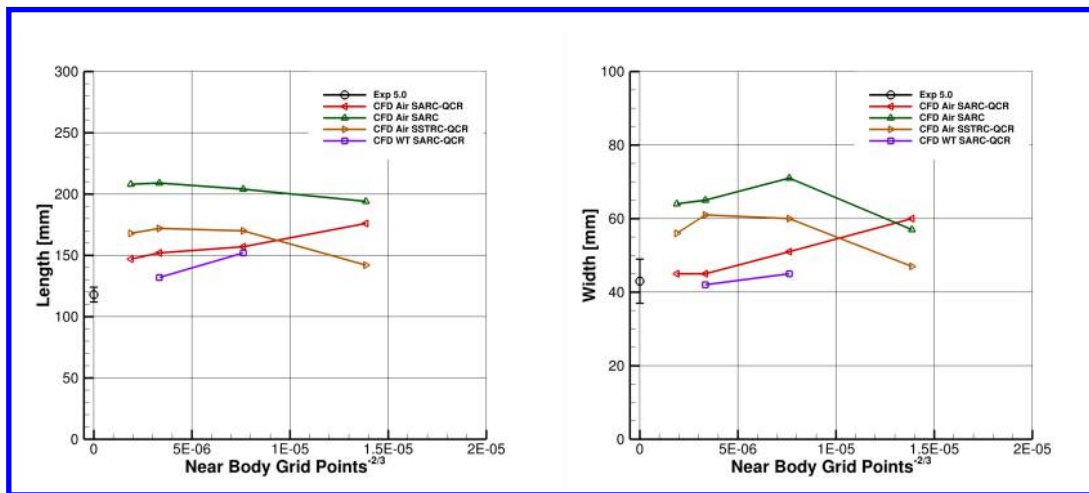
Figures 7 and 8 show the separation bubble size as a function of near body grid density, for all the cases at $\alpha = 5.0^\circ$ and $\alpha = -2.5^\circ$. The experimental values with uncertainties are shown along the vertical axis. The CFD Air cases all over-predict the bubble size, when compared to the experimental values. Sweeps were run with three different turbulence models, and will be further discussed Section IV.C. SARC predicted the largest bubble sizes, followed by SSTRC-QCR, and lastly SARC-QCR. The cases run with wind tunnel walls also predicted smaller bubble sizes than their similar air case. The cases with the wind tunnel walls also seem to extrapolate to the experimental data values.

Figures 9 and 10 show coefficient of pressure slices at various stations on the model, for all the cases run (with SARC-QCR). Note that experimental surface pressure data from the test have not been fully processed as of the time of this writing. Therefore, these C_P comparisons should be considered preliminary. For the $\alpha = 5.0^\circ$ case, most of the differences are at the leading edge, at the juncture flow region in the separation bubble, and at the wing tip. Higher grid densities lead towards a higher peak in pressure on the leading edge. Results are shown for the free air grid refinement compared with the wind tunnel medium and fine grid cases. The JFM grids are the same between the free air to wind tunnel sting-mast (WT+ST) medium and fine cases. Tip loading seems to be increased as the grids refine, due to the



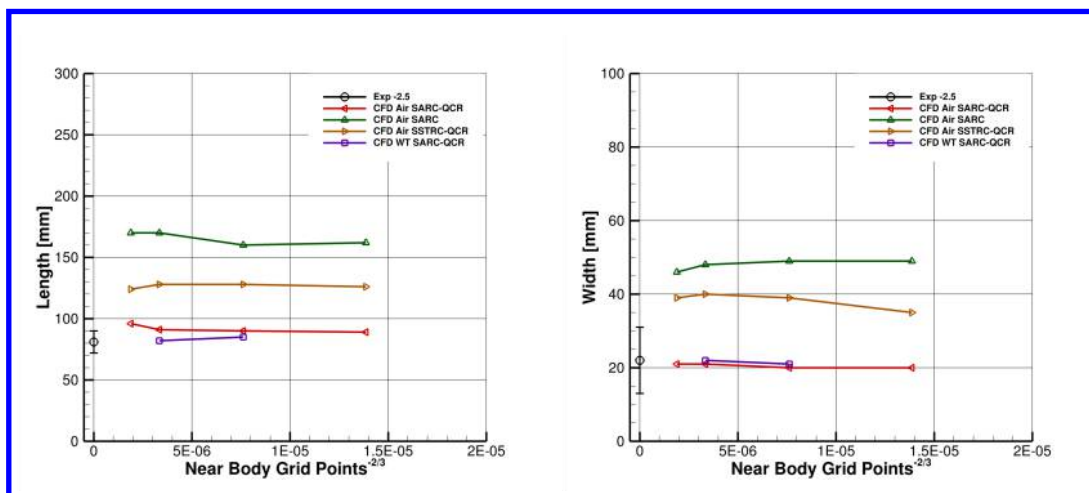
(a) Side-of-body separation example $\alpha = 5.0^\circ$ (b) Side-of-body separation example $\alpha = -2.5^\circ$

Figure 6. Typical side-of-body separation, CFD surface streamlines.



(a) Separation length at $\alpha = 5.0^\circ$ (b) Separation width at $\alpha = 5.0^\circ$

Figure 7. Separation size as a function of grid density and turbulence model $\alpha = 5.0^\circ$.



(a) Separation length at $\alpha = -2.5^\circ$ (b) Separation width at $\alpha = -2.5^\circ$

Figure 8. Separation size as a function of grid density and turbulence model $\alpha = -2.5^\circ$.

increased resolution of the wing tip vortex and its influence on tip loading. The CFD $\alpha = 5.0^\circ$ cases with the wind tunnel walls seem to have higher peaks than the free air case. Similarity, the CFD $\alpha = -2.5^\circ$ cases with wind tunnel walls show differences on the pressure side of the wing. Both can probably be attributed to wind tunnel wall effects.

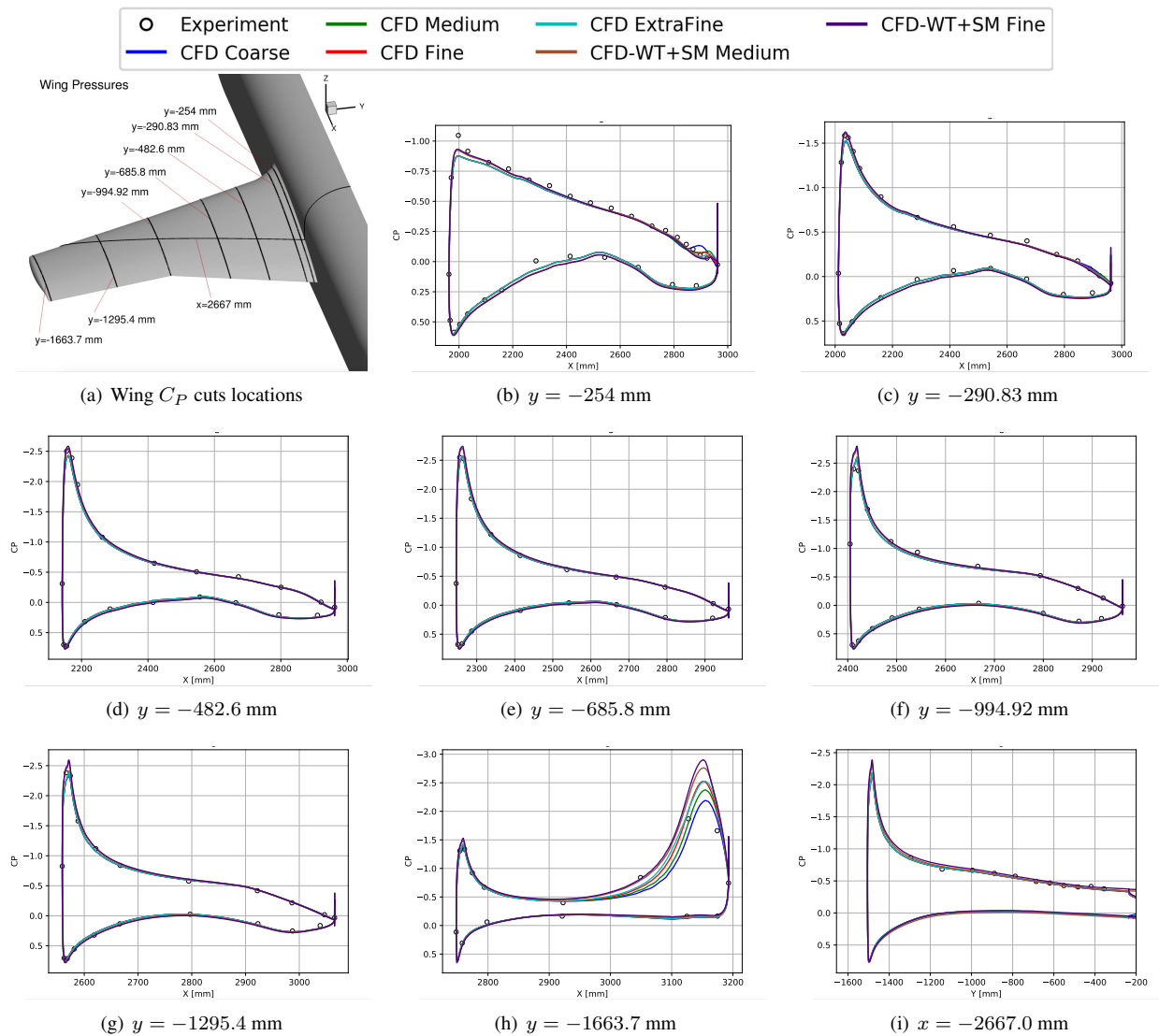


Figure 9. C_P slices for $\alpha = 5.0^\circ$ for all CFD grids (SARC-QCR).

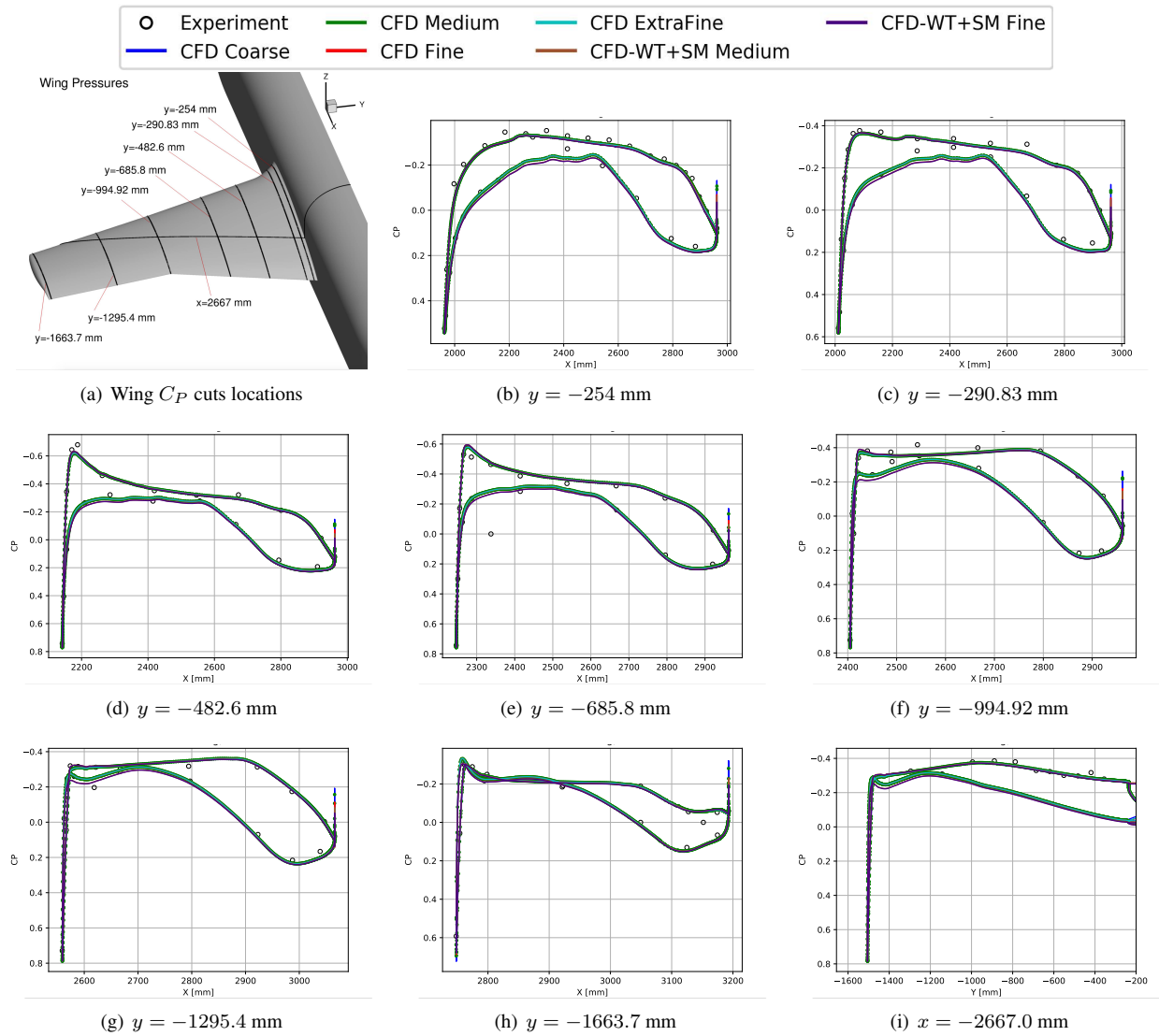


Figure 10. C_P slices for $\alpha = -2.5^\circ$ for all CFD grids (SARC-QCR).

A. CFD Free Air Grid Sequence Comparisons

A series of grid levels, including a coarse, medium, fine, and extra-fine were run. For brevity, only the results run with SARC-QCR will be shown here. Figures 11 and 12 show the corresponding side of body separation bubble topology for the 4 levels of grid refinement. The size of the bubble seems very similar in the fine and extrafine cases, yet the surface streamlines are different, suggesting that the flow is very much three dimensional.

Figures 13 and 14 show slice contours of velocity and Reynolds stresses in the trailing edge region for the medium and fine grid. These slices also correspond approximately to the regions where the LDV data were taken. The three dimensional bubble size for the medium grid looks slightly larger than the fine grid.

Comparisons between the experimental LDV measurements and CFD (grid refinement air cases) extracted velocities and Reynolds stresses are shown in Figs. 15 to 20 for $\alpha = 5.0^\circ$, and Figs. 21 to 26 for $\alpha = -2.5^\circ$. The top picture in each figure shows CFD surface streamlines highlighting the juncture flow region, and the red line represents the extracted profile line. The velocities in the regions leading up to the separation bubble agree very well with the LDV data. There is almost no variation due to grid resolution, for the velocities and Reynolds stresses, with the exception of the coarse grid, which stands out versus the rest of the finer grids.

Reynolds stresses do compare fairly well in regions upstream of the separation bubble. Notably, $v'v'$ seems to be over-predicted at all the grid resolutions, while $u'w'$ is both under-predicted and over-predicted. The values of $u'u'$

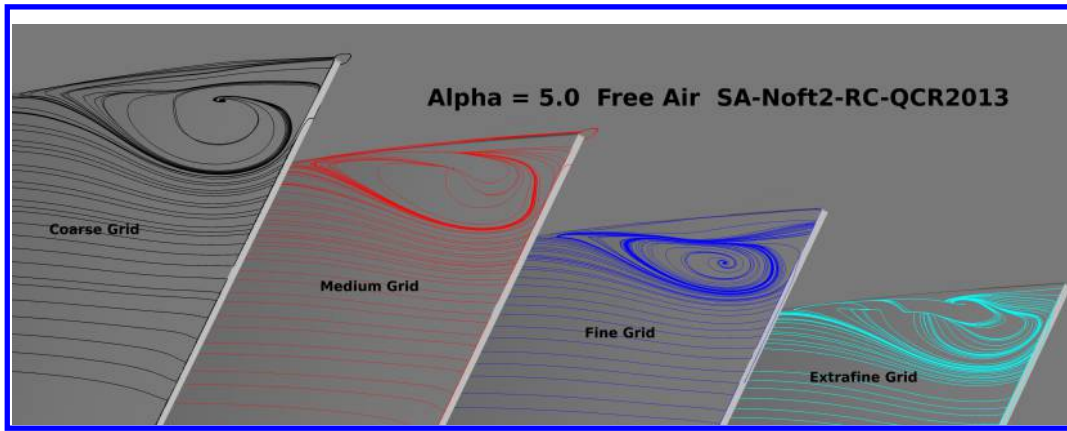


Figure 11. Side of body separation bubble topology vs grid refinement $\alpha = 5.0^\circ$.

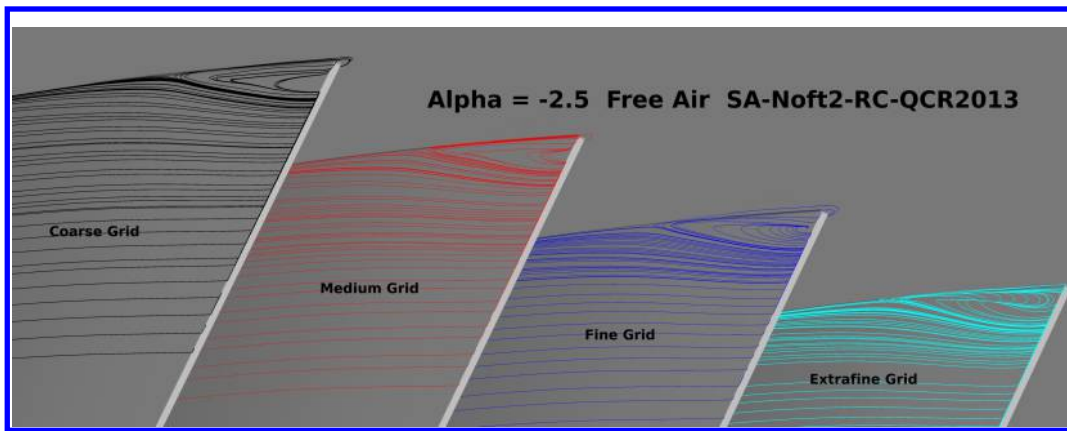


Figure 12. Side of body separation bubble topology vs grid refinement $\alpha = -2.5^\circ$.

are under-predicted in the regions upstream of the separation bubble, as seen in Fig. 17 and Fig. 23, yet $u'u'$ does match better away from the wall just $30mm$ away from the fuselage, in Fig. 18 and Fig. 24.

Figure 19 and Fig. 25 are both located close to the start of the separation. Both show that the CFD is starting to predict some form of separation, contrary to the experiment. The velocities and Reynolds stresses show no signs of correlation in Fig. 20 and Fig. 26, often over-predicting the experiment in magnitude in the separation region. The reverse flow region seems to get closer to the wing surface as the grid resolution increases, though this trend stops around the fine grid level.

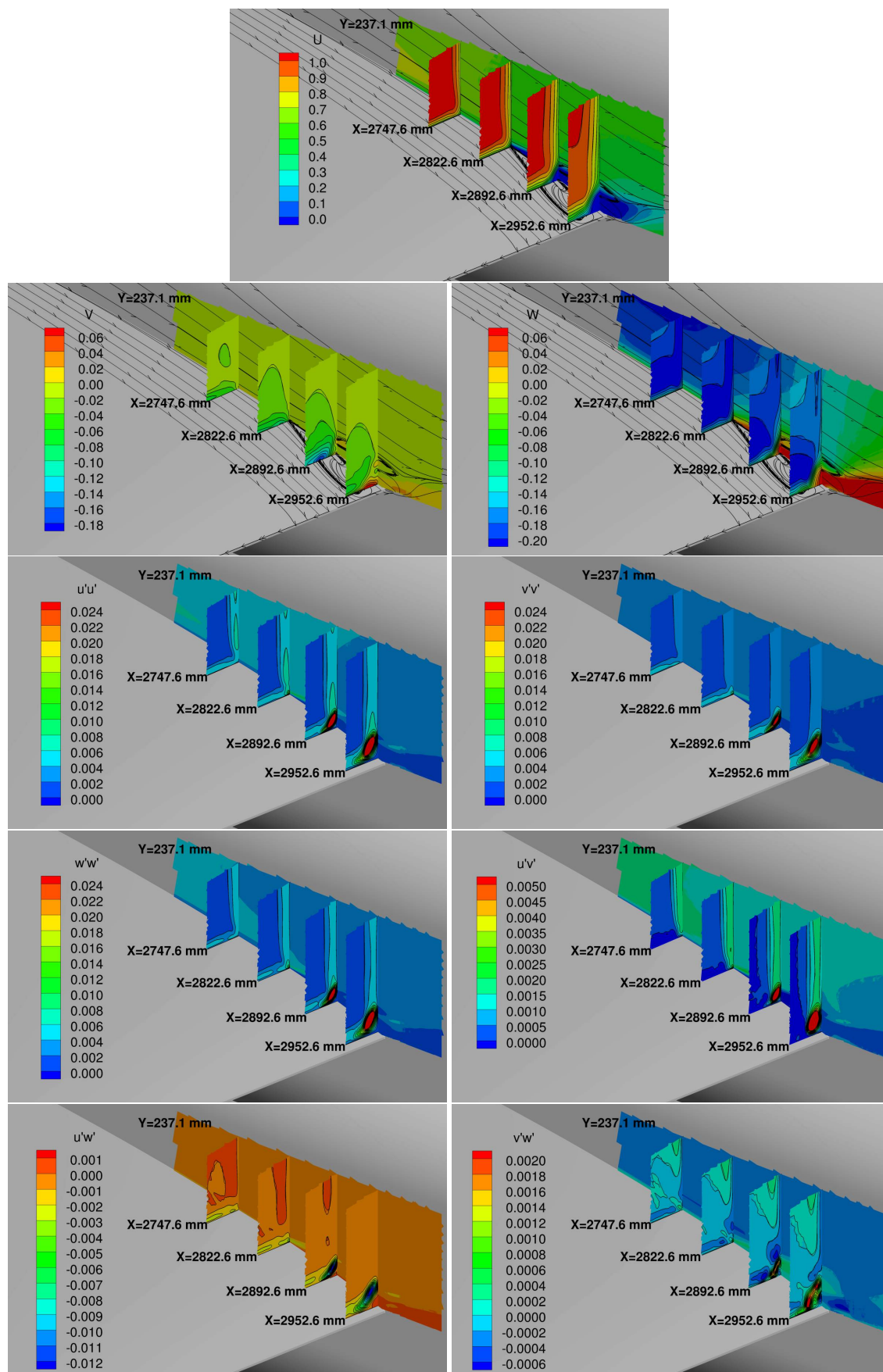


Figure 13. Velocity and Reynolds Stresses in trailing edge junction, CFD Air Medium grid at $\alpha = 5.0^\circ$.

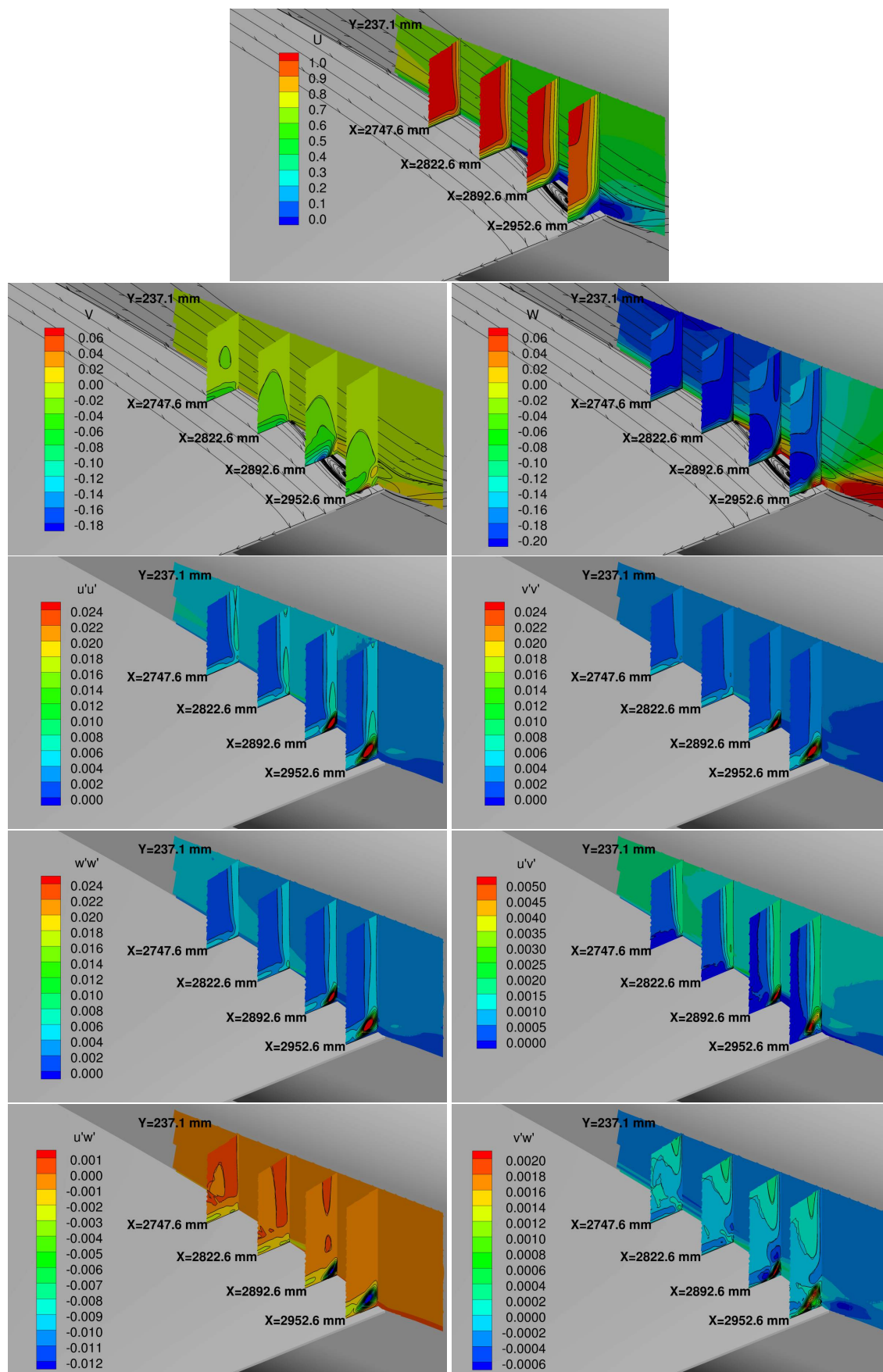


Figure 14. Velocity and Reynolds Stresses in trailing edge junction, CFD Air Fine grid at $\alpha = 5.0^\circ$.

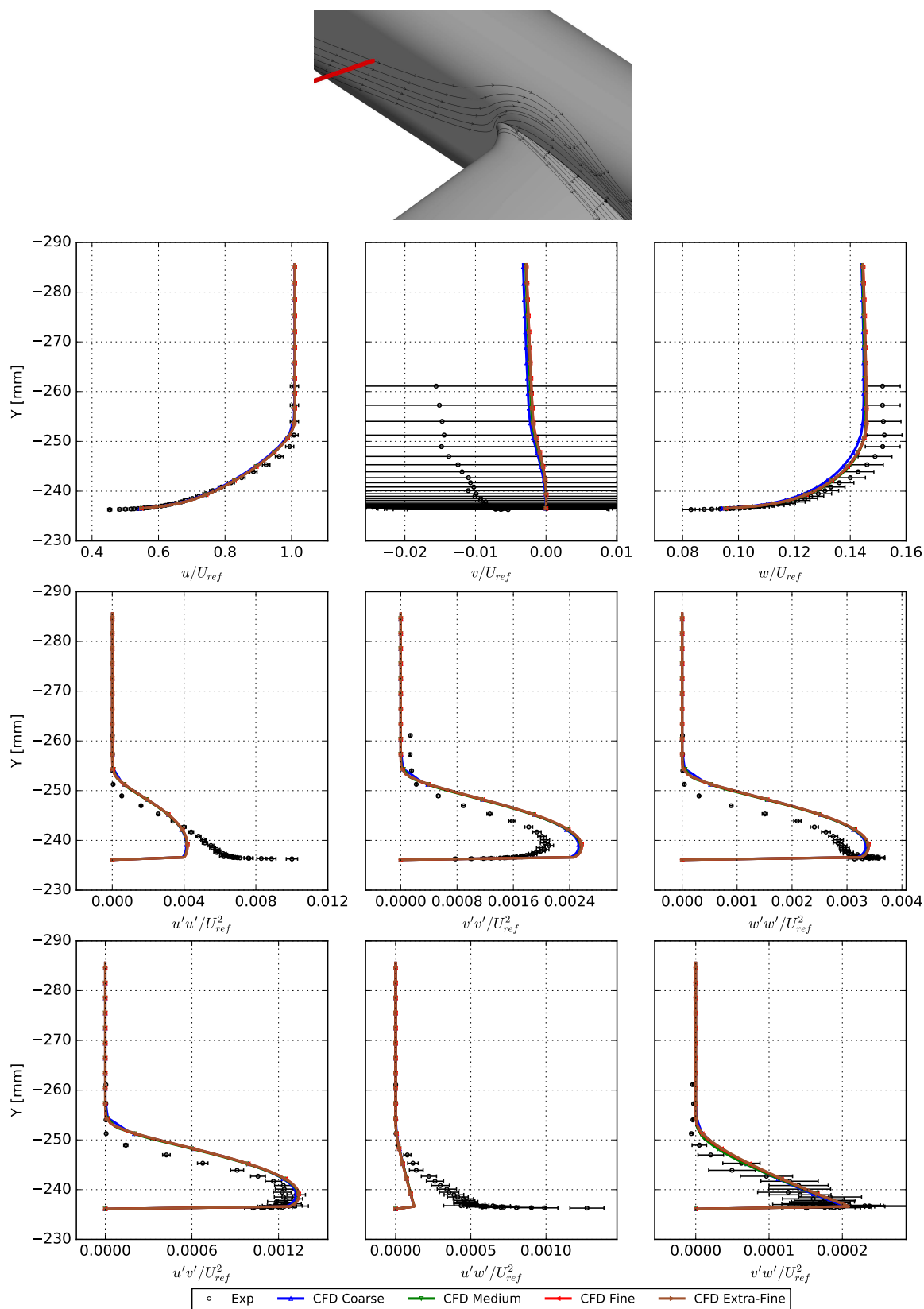


Figure 15. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 1168.4$, $z = 0.0$, just past nose of fuselage.

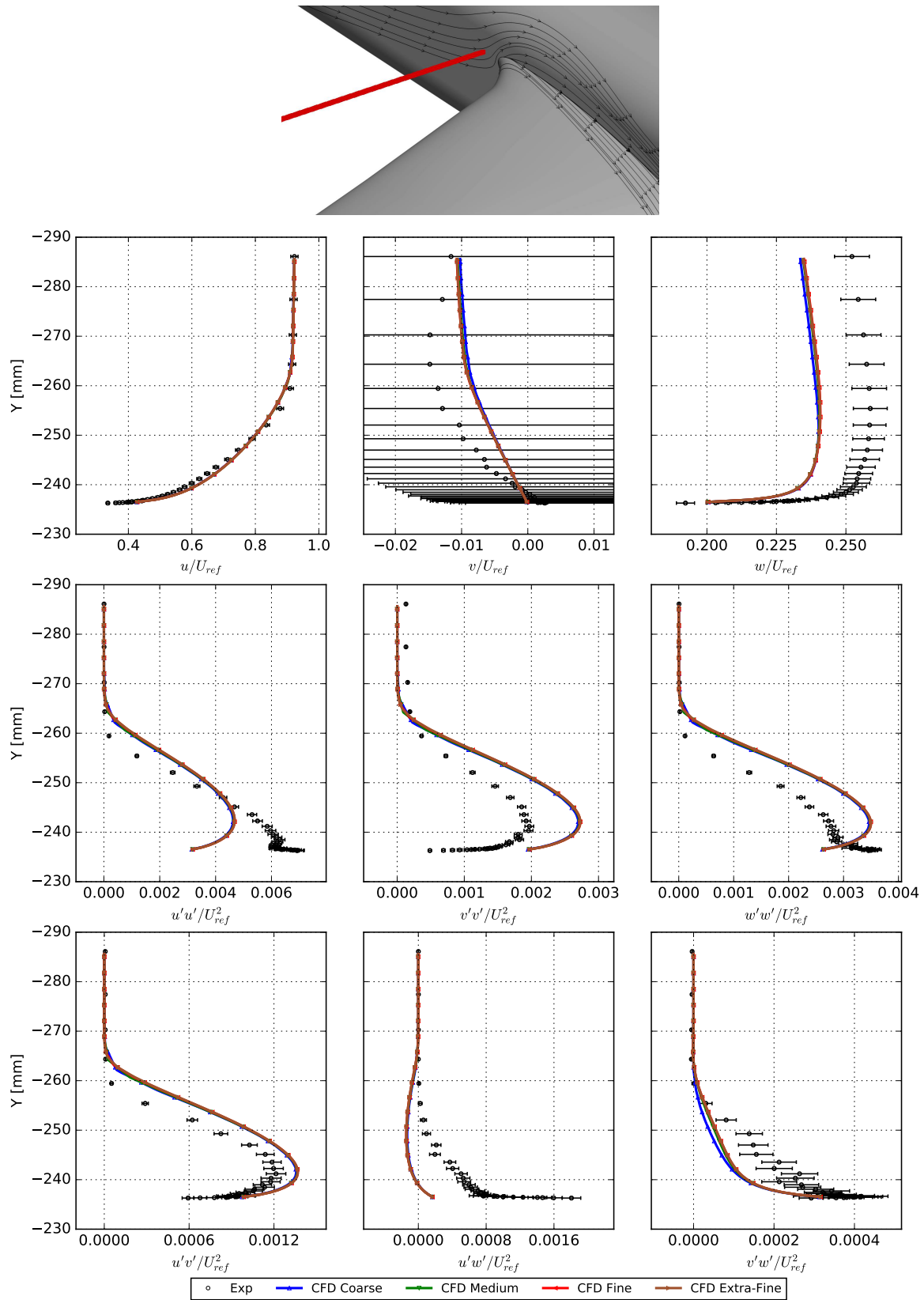


Figure 16. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 1859.2$, $z = 55.05$, just upstream of the LE.

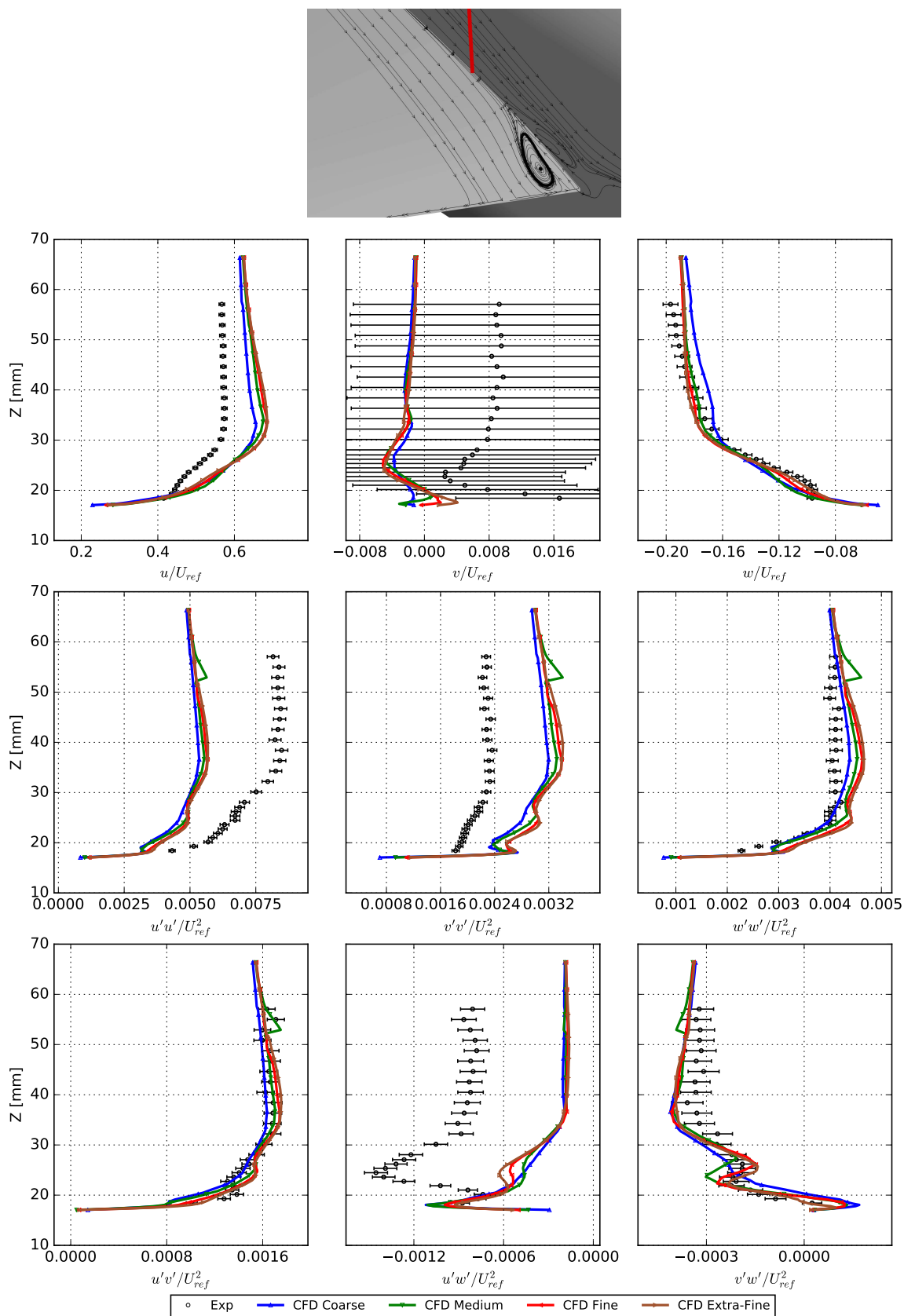


Figure 17. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2747.6$, $y = 237.1$, upstream of separation, 1 mm from fuselage.

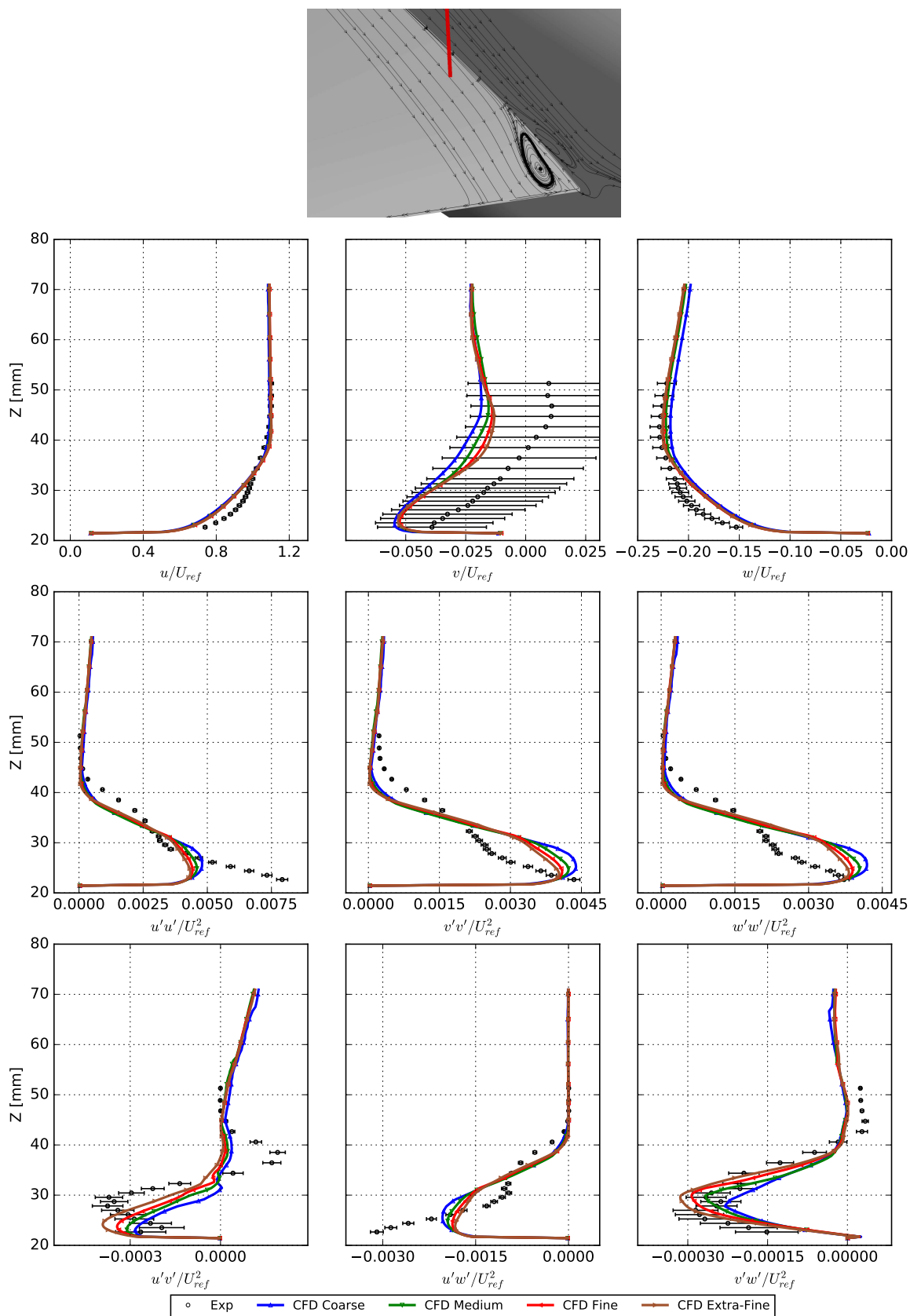


Figure 18. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2747.6$, $y = 266.1$, upstream of separation, 30 mm from fuselage.

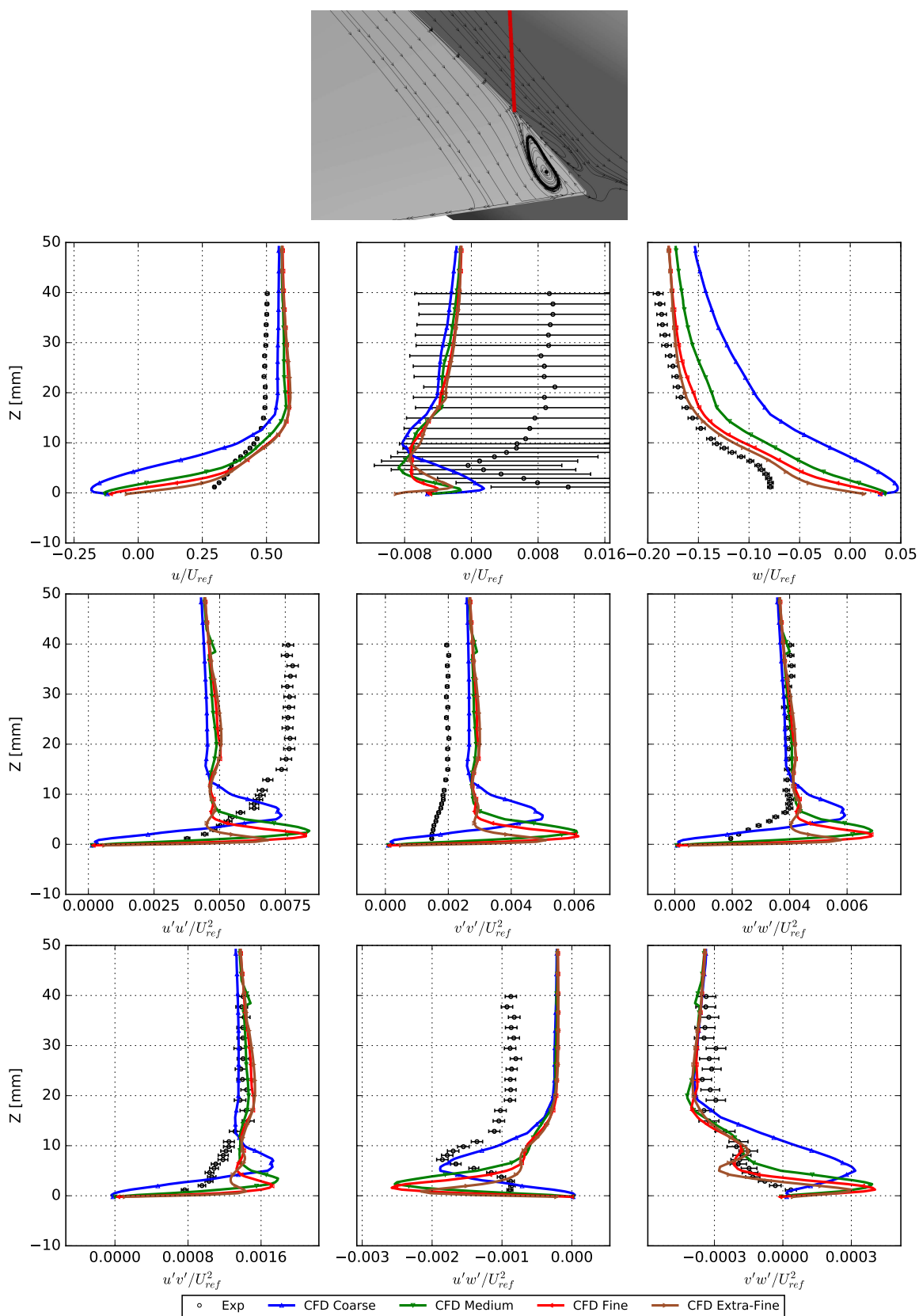


Figure 19. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2822.6$, $y = 237.1$, close to start of separation, 1 mm from fuselage.

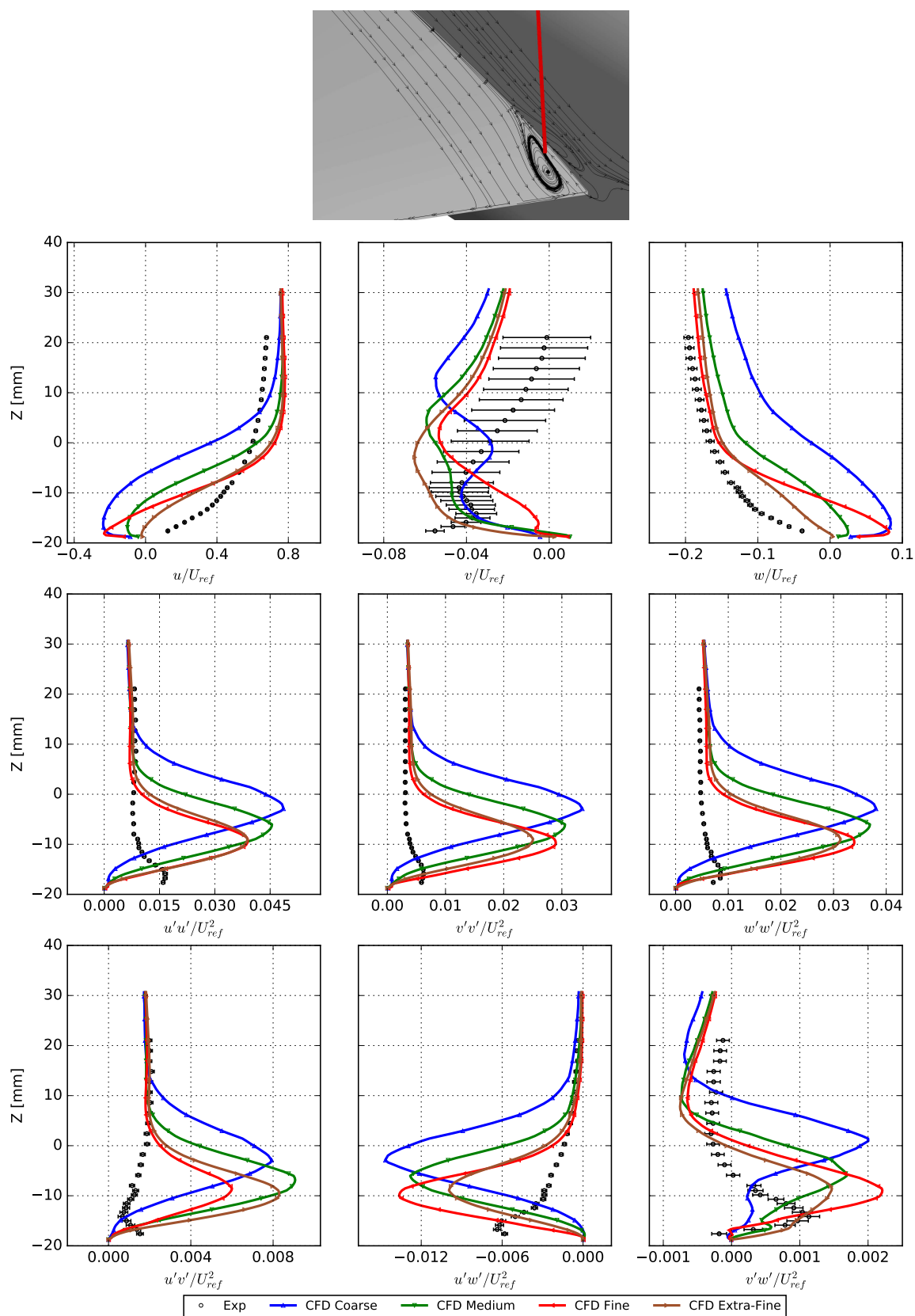


Figure 20. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2892.6$, $y = 246.1$, in the separation bubble.

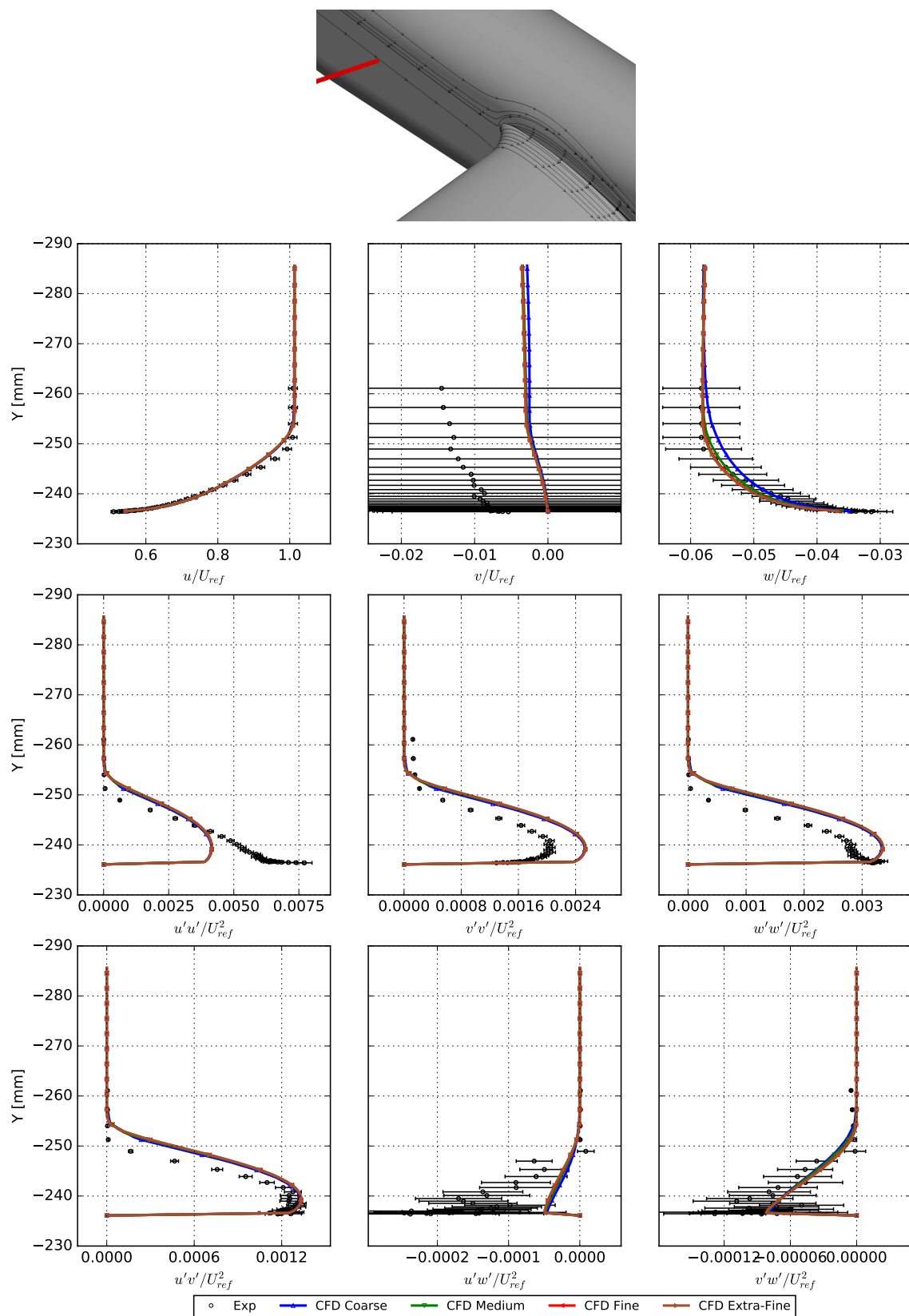


Figure 21. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = -2.5^\circ$, $x = 1168.4$, $z = 0.0$, just past nose of fuselage.

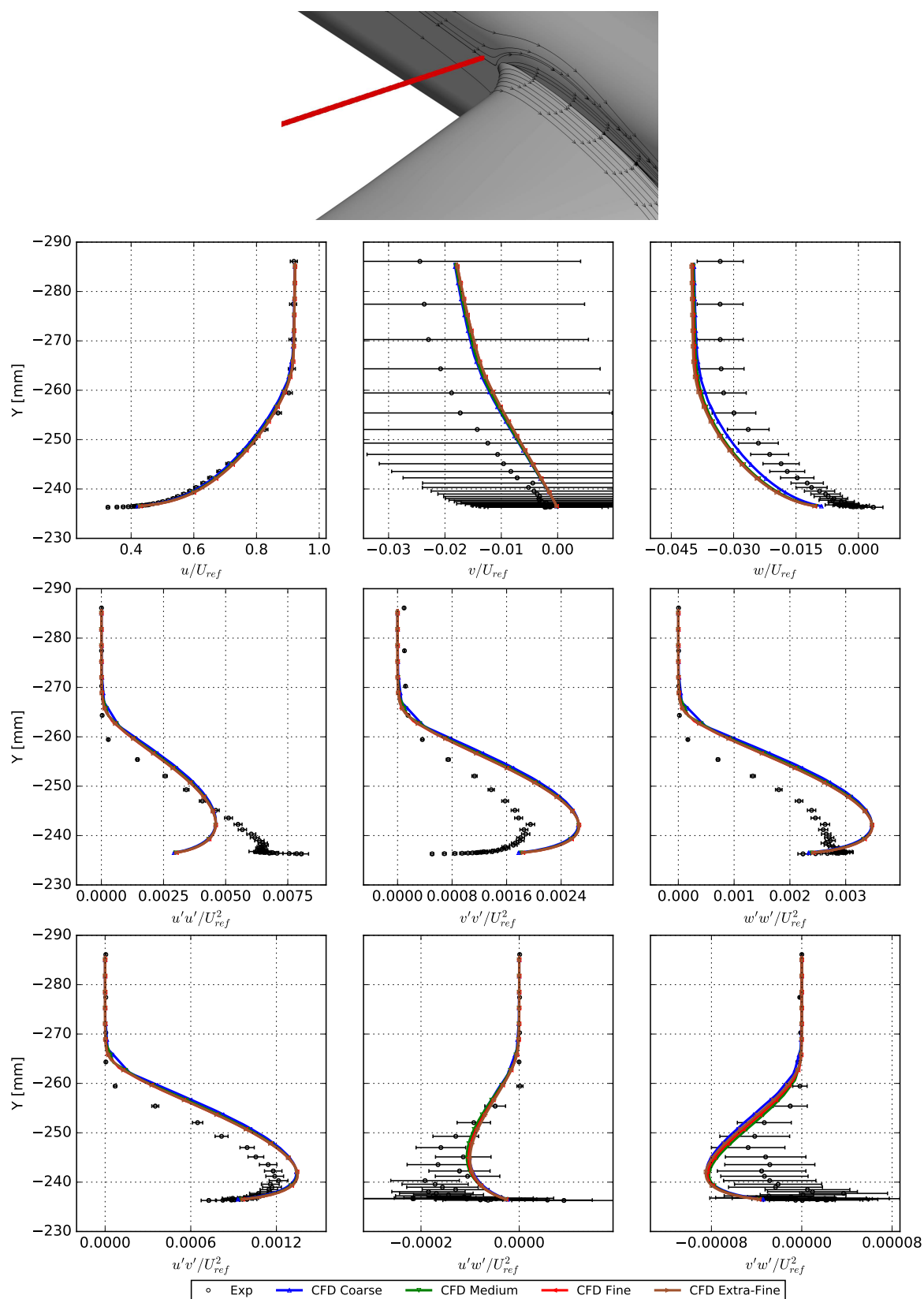


Figure 22. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = -2.5^\circ$, $x = 1859.2$, $z = 55.05$, just upstream of LE.

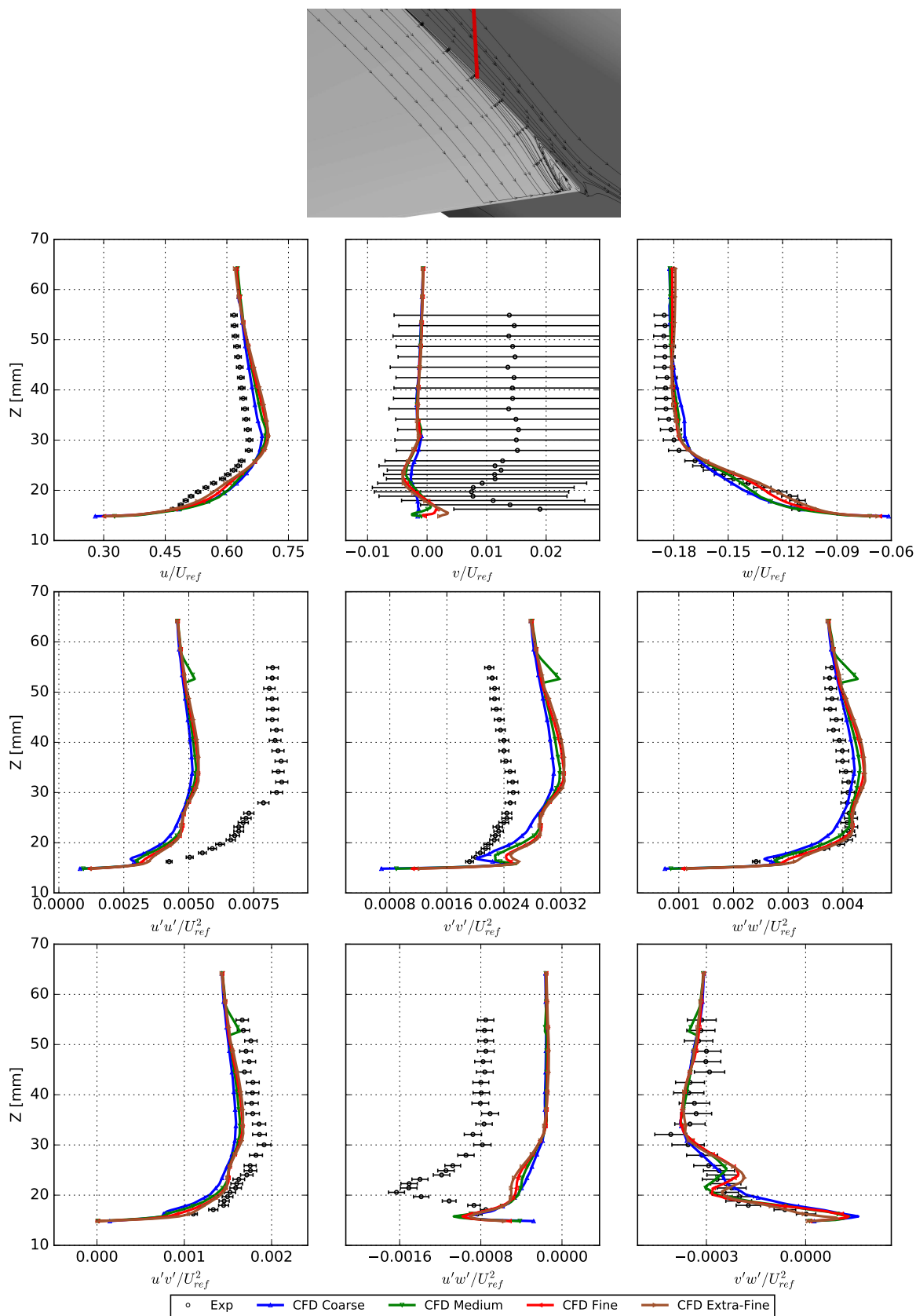


Figure 23. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = -2.5^\circ$, $x = 2757.6$, $y = 237.1$, upstream of separation, 1 mm from fuselage.

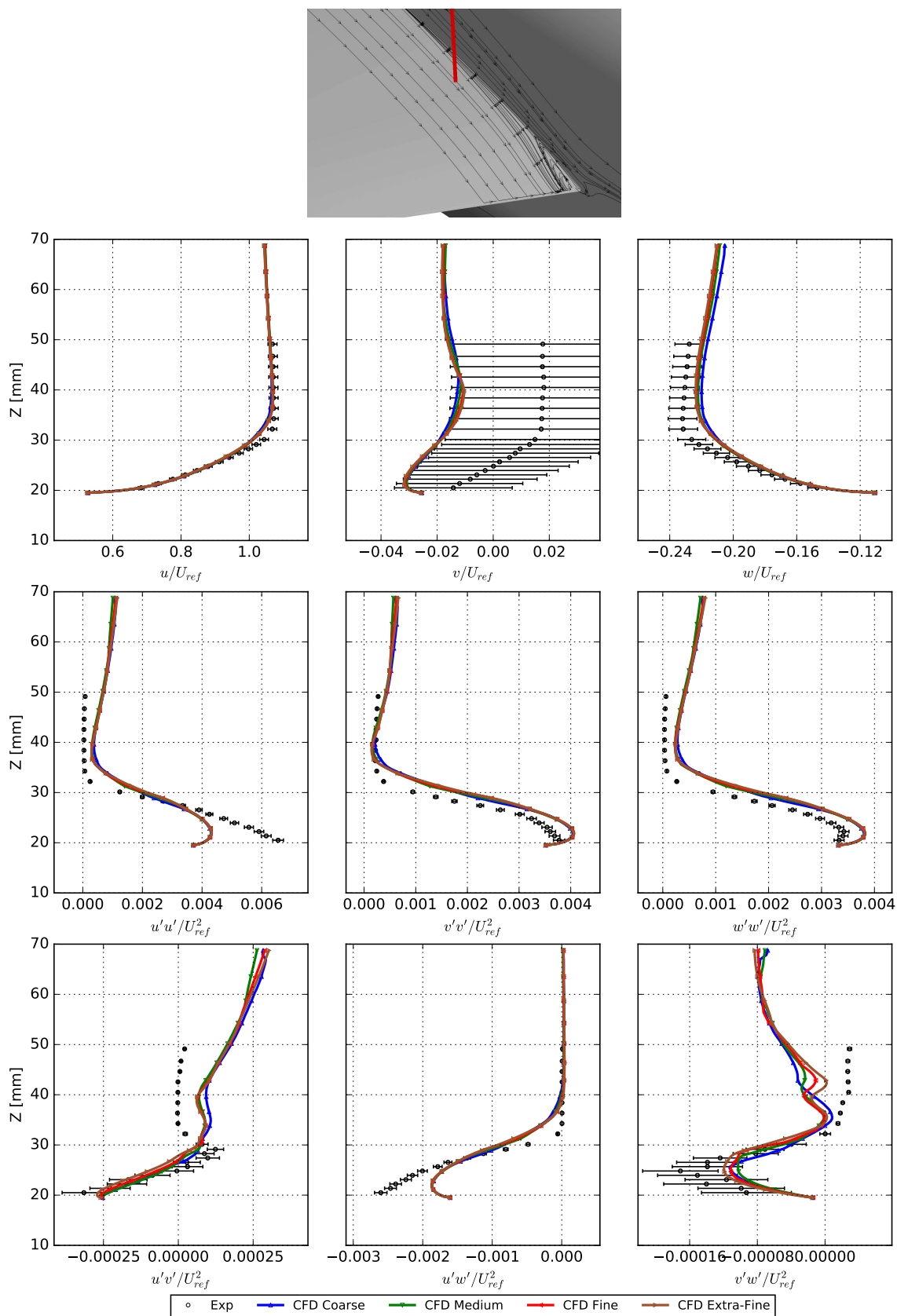


Figure 24. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = -2.5^\circ$, $x = 2757.6$, $y = 266.1$, upstream of separation, 30 mm from fuselage.

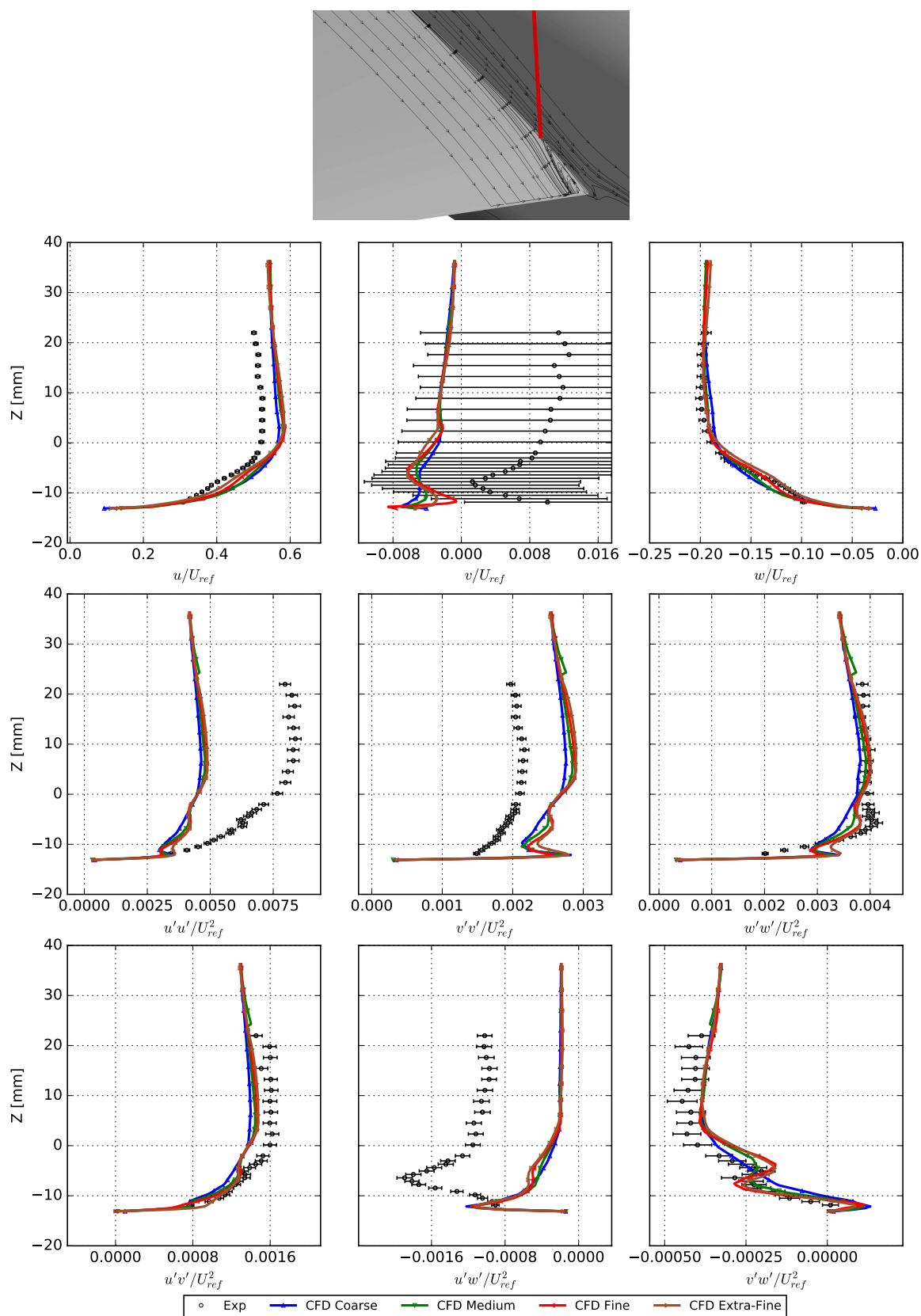


Figure 25. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = -2.5^\circ$, $x = 2869.6$, $y = 237.1$, upstream of separation, 1 mm from fuselage.

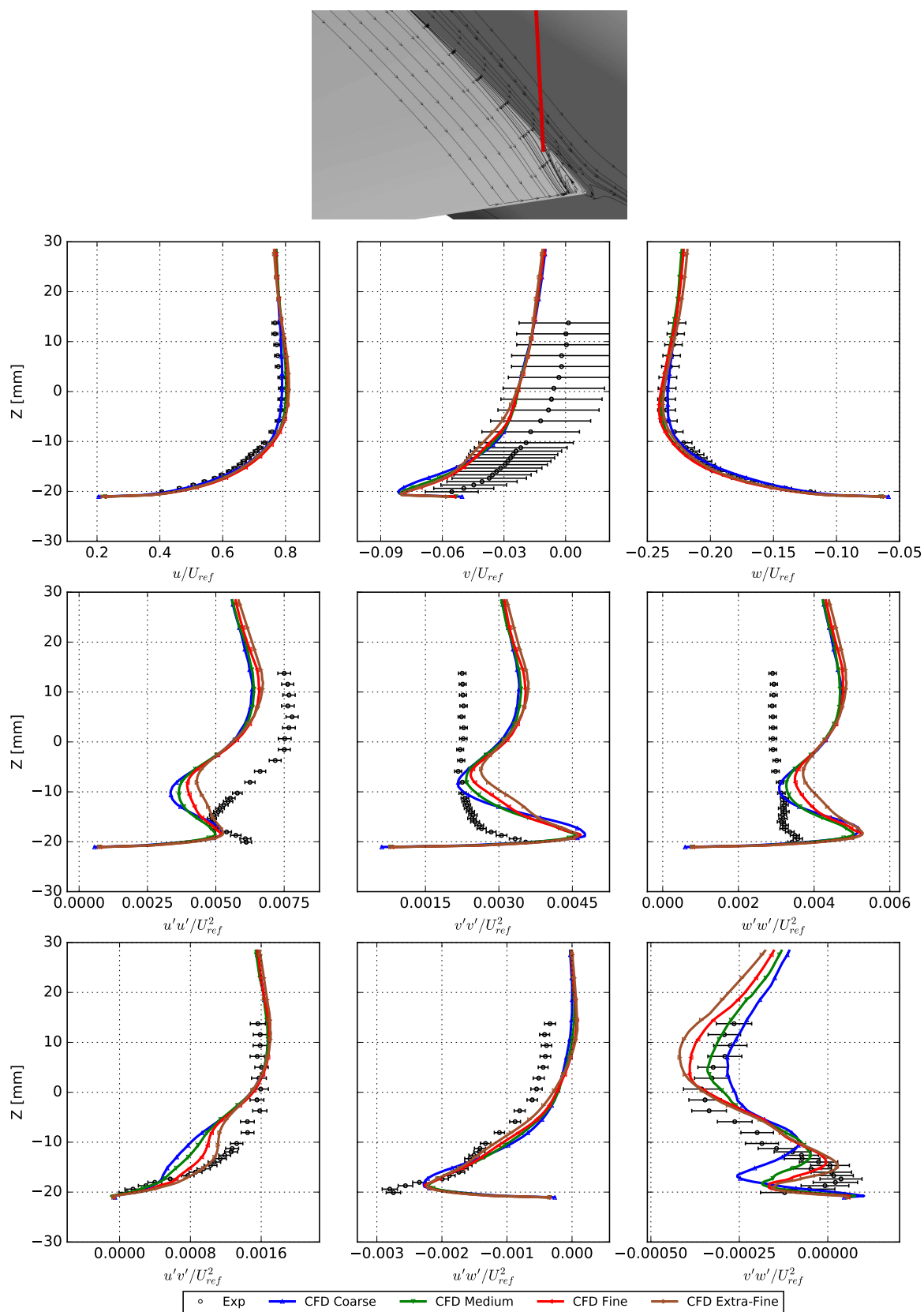
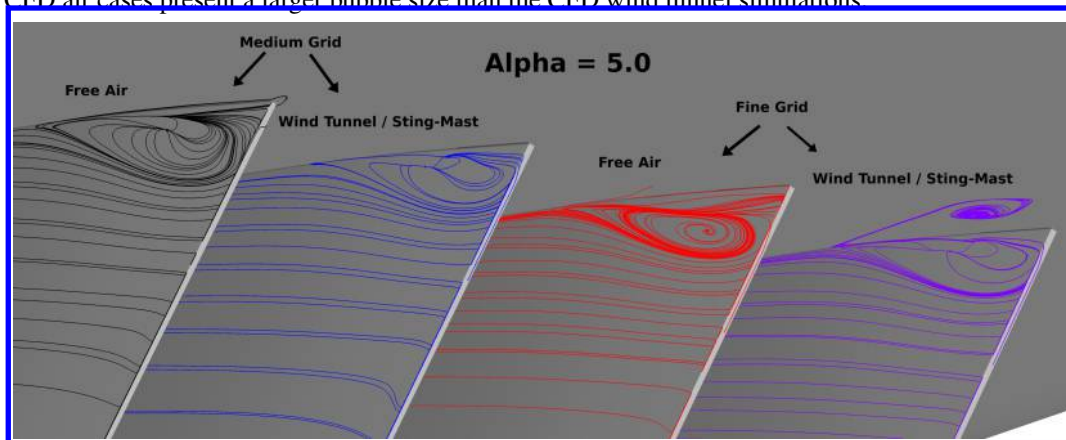


Figure 26. Grid Refinement Comparison (CFD Air): Velocities and Reynolds Stresses at $\alpha = -2.5^\circ$, $x = 2899.6$, $y = 246.1$, at the start of the separation bubble.

B. CFD Wind Tunnel Wall Effects

A preliminary investigation of the wind tunnel wall effect on the juncture flow region is covered in this section. The exact same near body grids used in the CFD air medium and fine grid simulations are used and embedded into the 14x22 wind tunnel. The hope is that using the same near body grids can help isolate some of the wind tunnel modeling effects on the juncture flow region. An effort was made to keep the spacing similar in the test section, as the CFD air cases, but the 14x22 tunnel grids are still going to be inherently finer, due to how the grids were constructed.

Figure 27 shows the separation topology for both the CFD air and CFD wind tunnel cases. The overall shape of the bubble for the same grid resolution is very similar. The medium grids show a larger bubble size than the fine grids, and the CFD air cases present a larger bubble size than the CFD wind tunnel simulations.



(a) Bubble topology for $\alpha = 5.0^\circ$

Figure 27. Side of body separation bubble topology, tunnel wall effect.

The contour plots of the velocities and Reynolds stresses in Figs 28 and 29 give a three dimensional picture of the bubble. The contours between the medium and fine grid are very similar. However, when compared to the free air case, Figs. 13 and 14, there are more differences. The bubble seems to be taller and slightly narrower in the wind tunnel, while shorter and wider in the corresponding air case. There are still many similarities throughout the contours.

Figures 30 to 35 show the velocity and Reynolds stress profiles for the air medium, air fine, wind tunnel medium, and wind tunnel fine grids. Overall, the CFD wind tunnel profiles are very similar to each other, while the CFD air results show a little more spread.

The profiles are nearly identical upstream of the wing, in Figs. 30 and 31, with only the w profile being different. The speed in the w direction is higher in the wind tunnel, and agrees with the experiment as well. Figures 32 and 33 show the profiles upstream of the separation on the wing. The velocity profiles are still very similar, while the Reynolds stress profiles are starting to differ between the CFD air and CFD wind tunnel. At the start of separation, in Fig. 34, the profiles start to differ greatly between the CFD air and CFD wind tunnel. The CFD wind tunnel cases only predict a slight separation, while the CFD air profiles show a separation. In the separation bubble, in Fig. 35, the velocity profiles for the CFD wind tunnel show good agreement with the experimental data. The Reynolds normal stress profiles do look similar, with larger magnitudes for the CFD air cases, but are much larger than the experimental data. Only the $v'w'$ Reynolds shear stress compare well with each other.

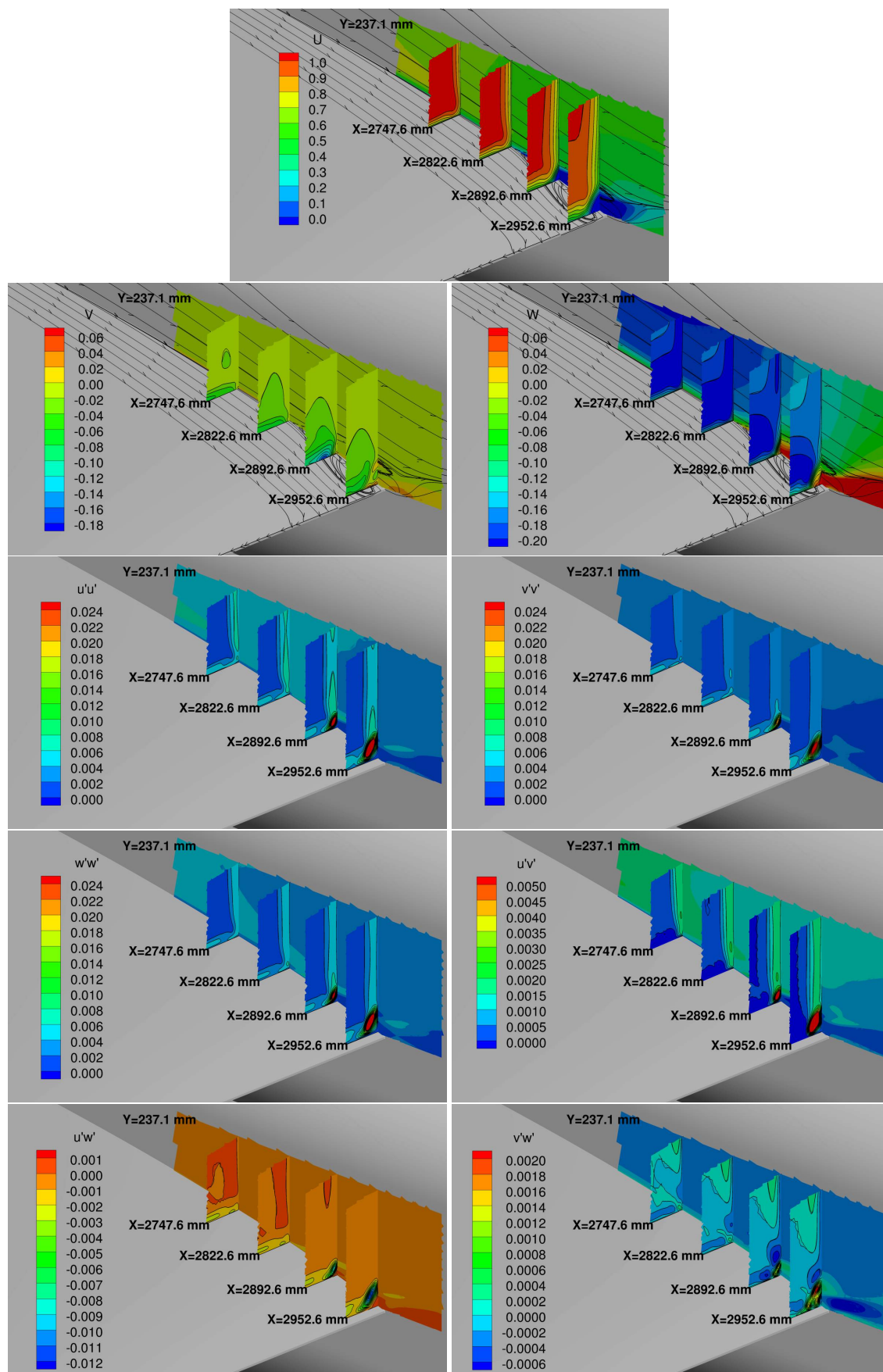


Figure 28. Velocity and Reynolds Stresses in trailing edge junction, CFD Wind Tunnel Medium grid at $\alpha = 5.0^\circ$.

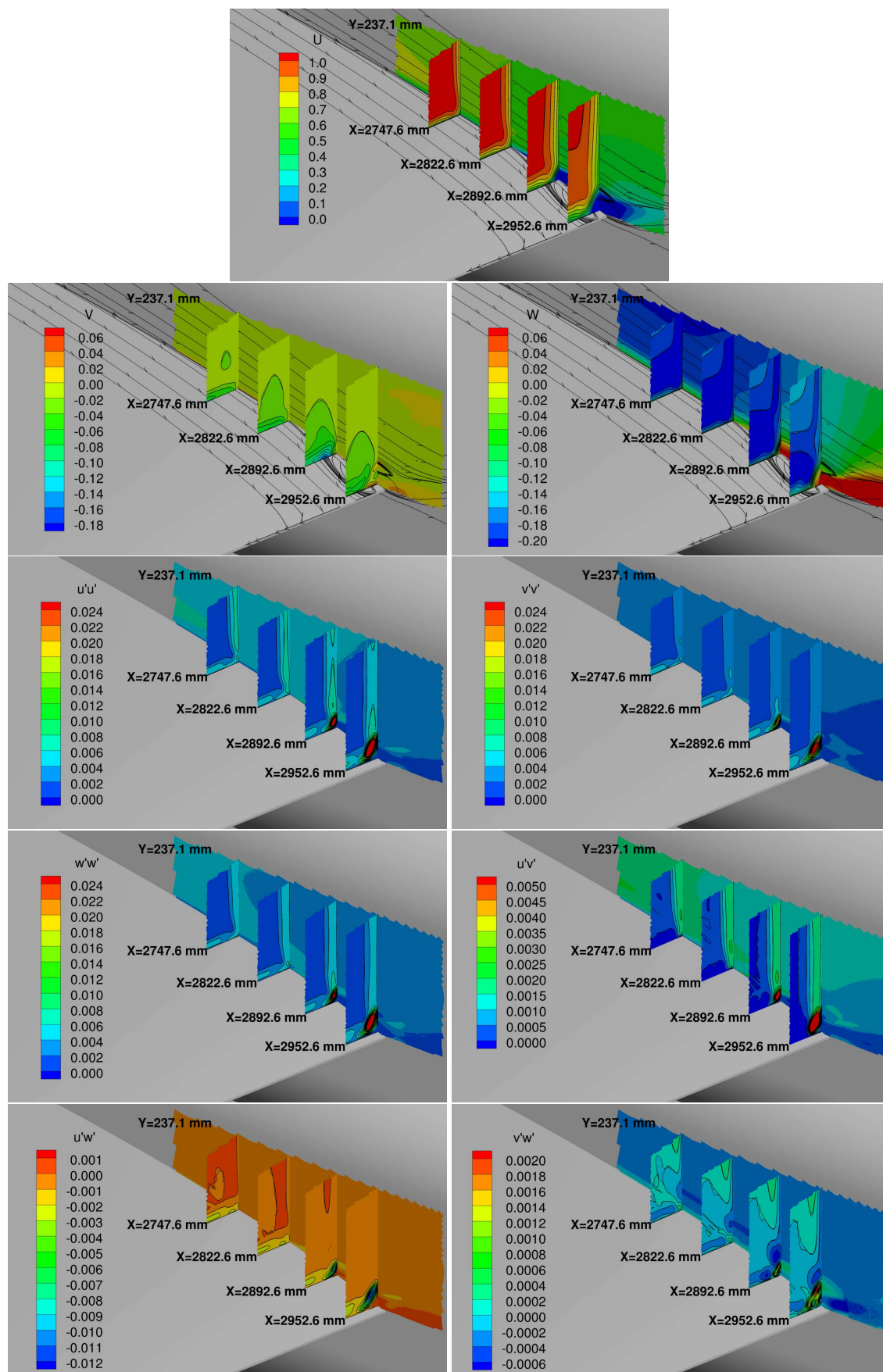


Figure 29. Velocity and Reynolds Stresses in trailing edge junction, CFD Wind Tunnel Fine grid at $\alpha = 5.0^\circ$.

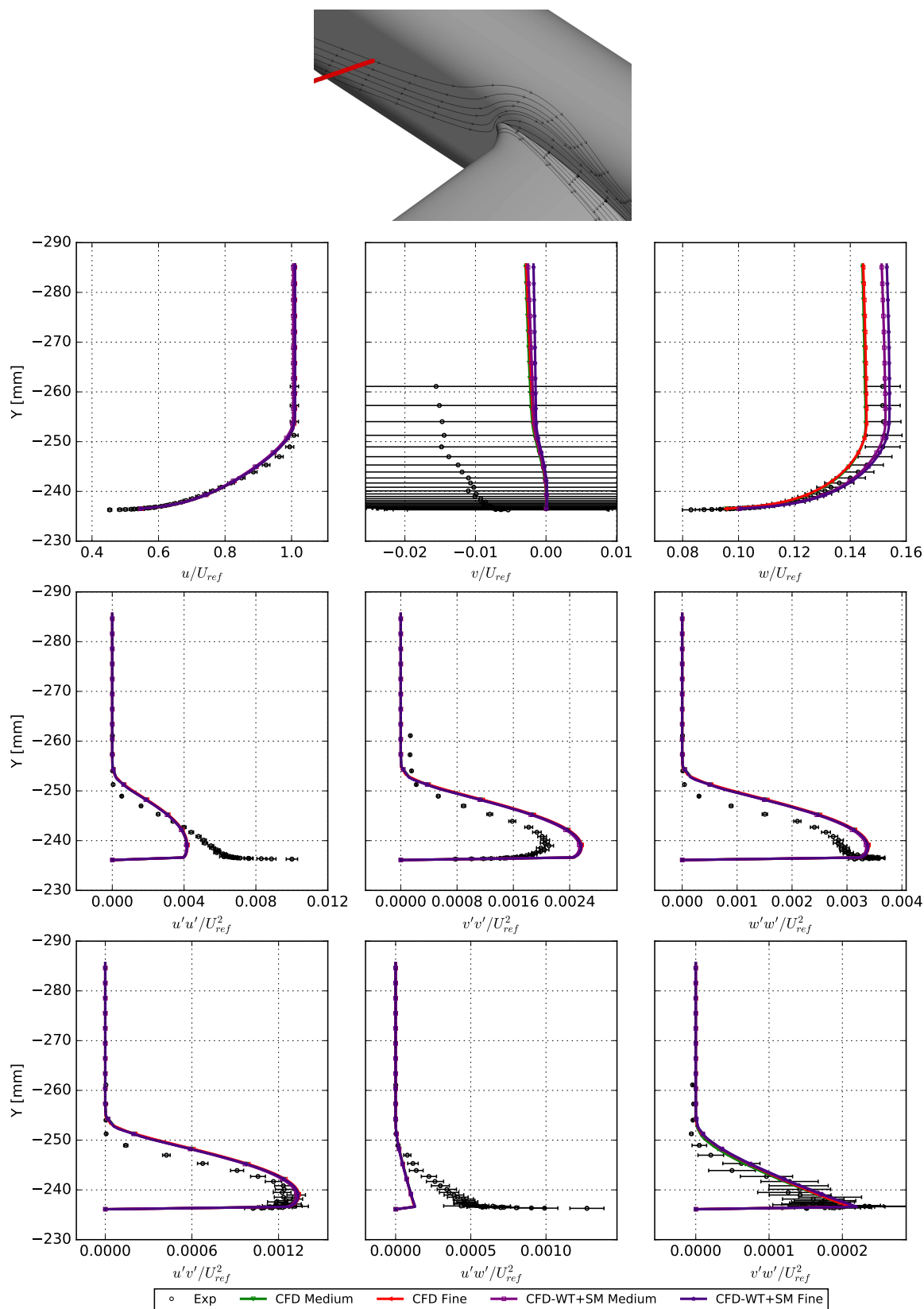


Figure 30. Tunnel Wall Effect Comparison Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 1168.4$, $z = 0.0$, just past nose of fuselage.

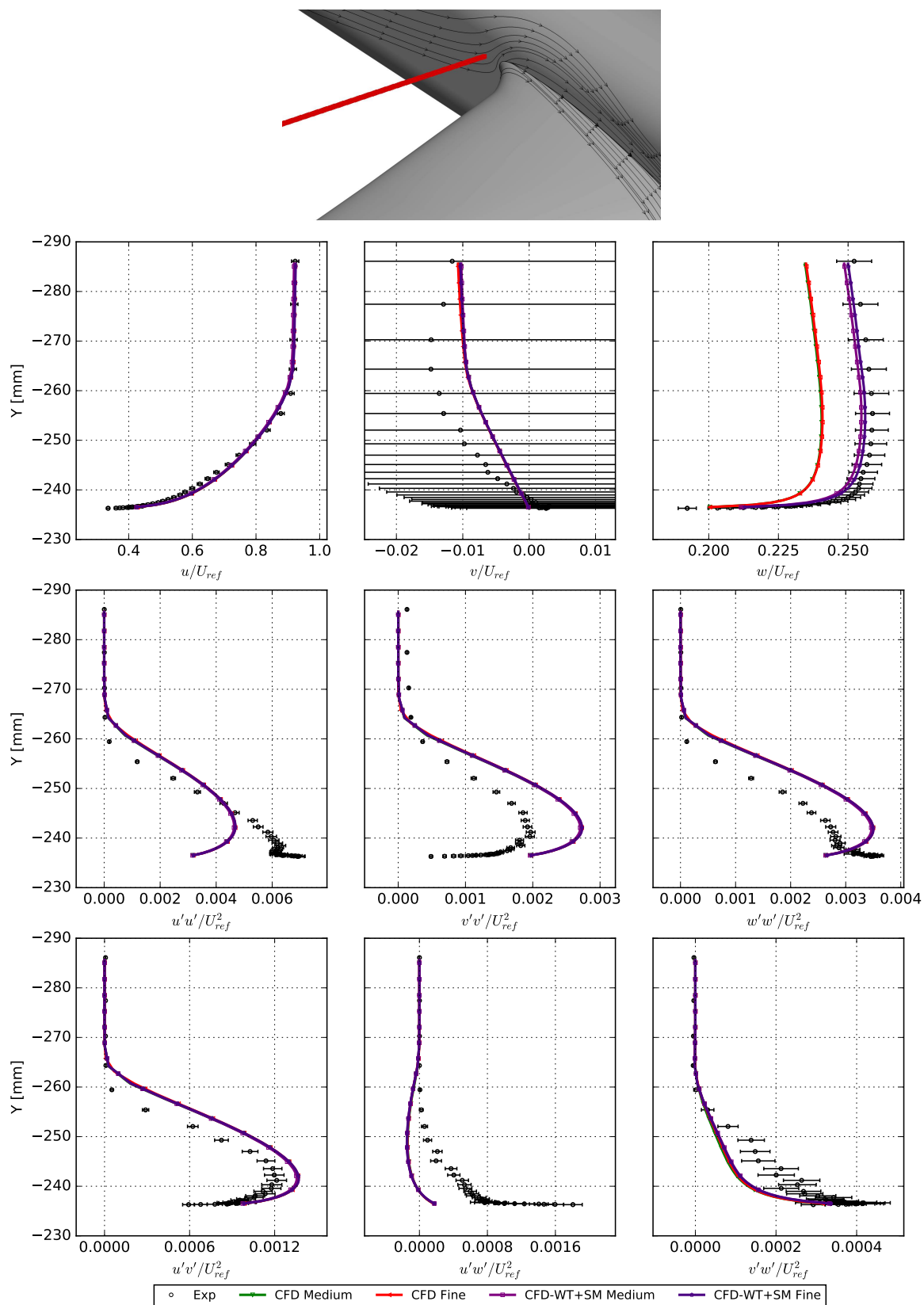


Figure 31. Tunnel Wall Effect Comparison Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 1859.2$, $z = 55.05$, just upstream of LE.

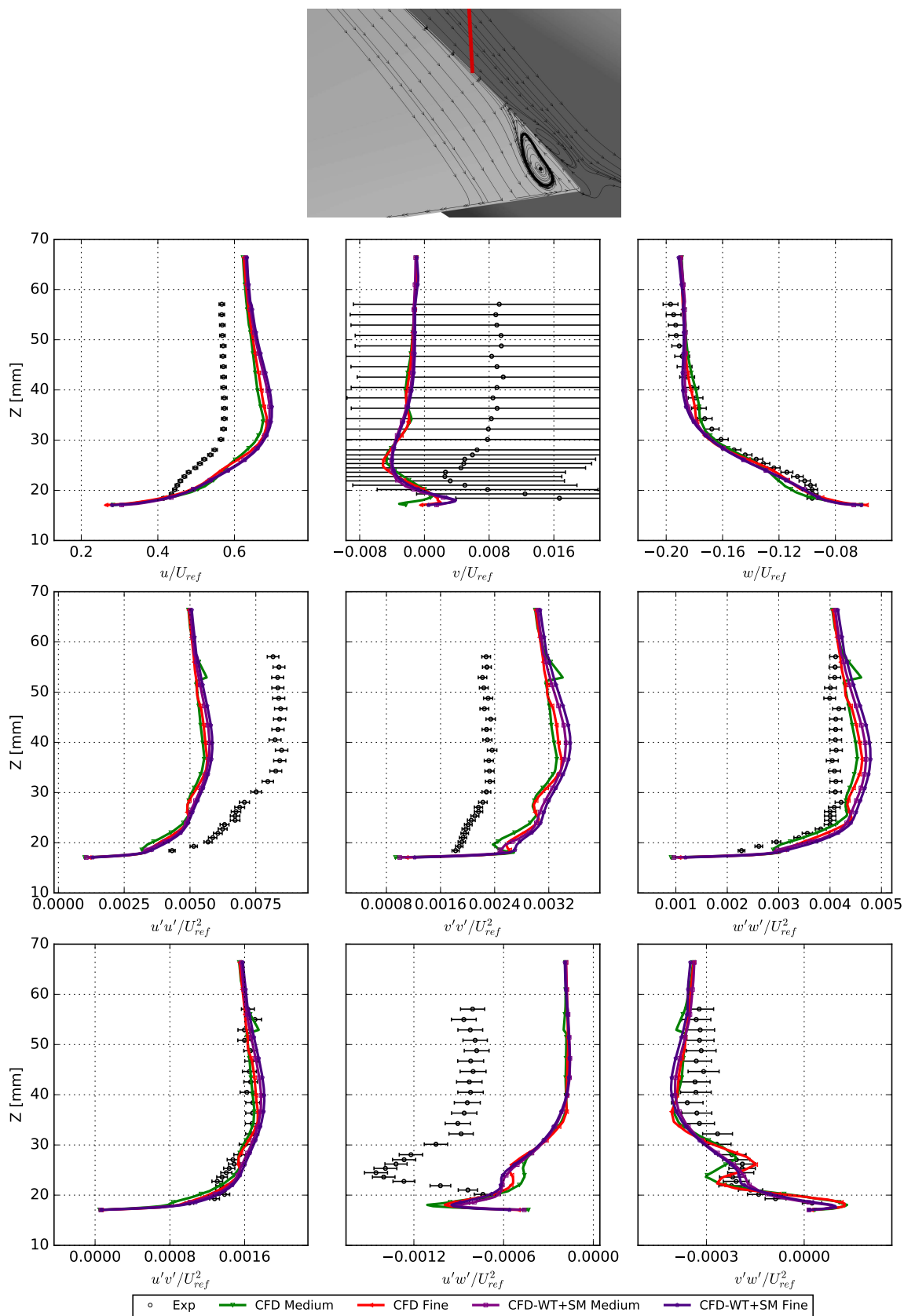


Figure 32. Tunnel Wall Effect Comparison Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2747.6$, $y = 237.1$, upstream of separation, 1 mm from fuselage.

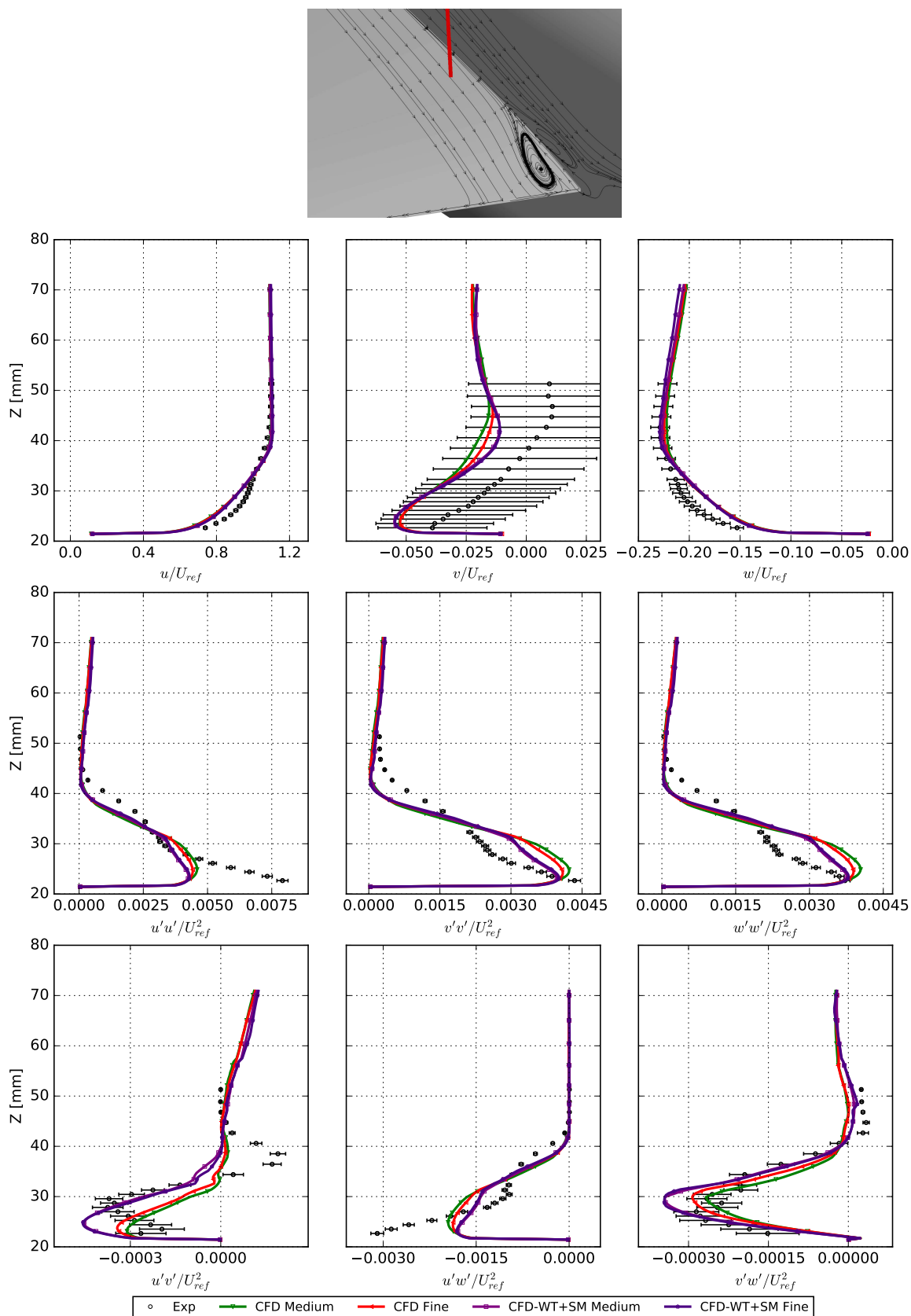


Figure 33. Tunnel Wall Effect Comparison Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2747.6$, $y = 266.1$, upstream of separation, 30 mm from fuselage.

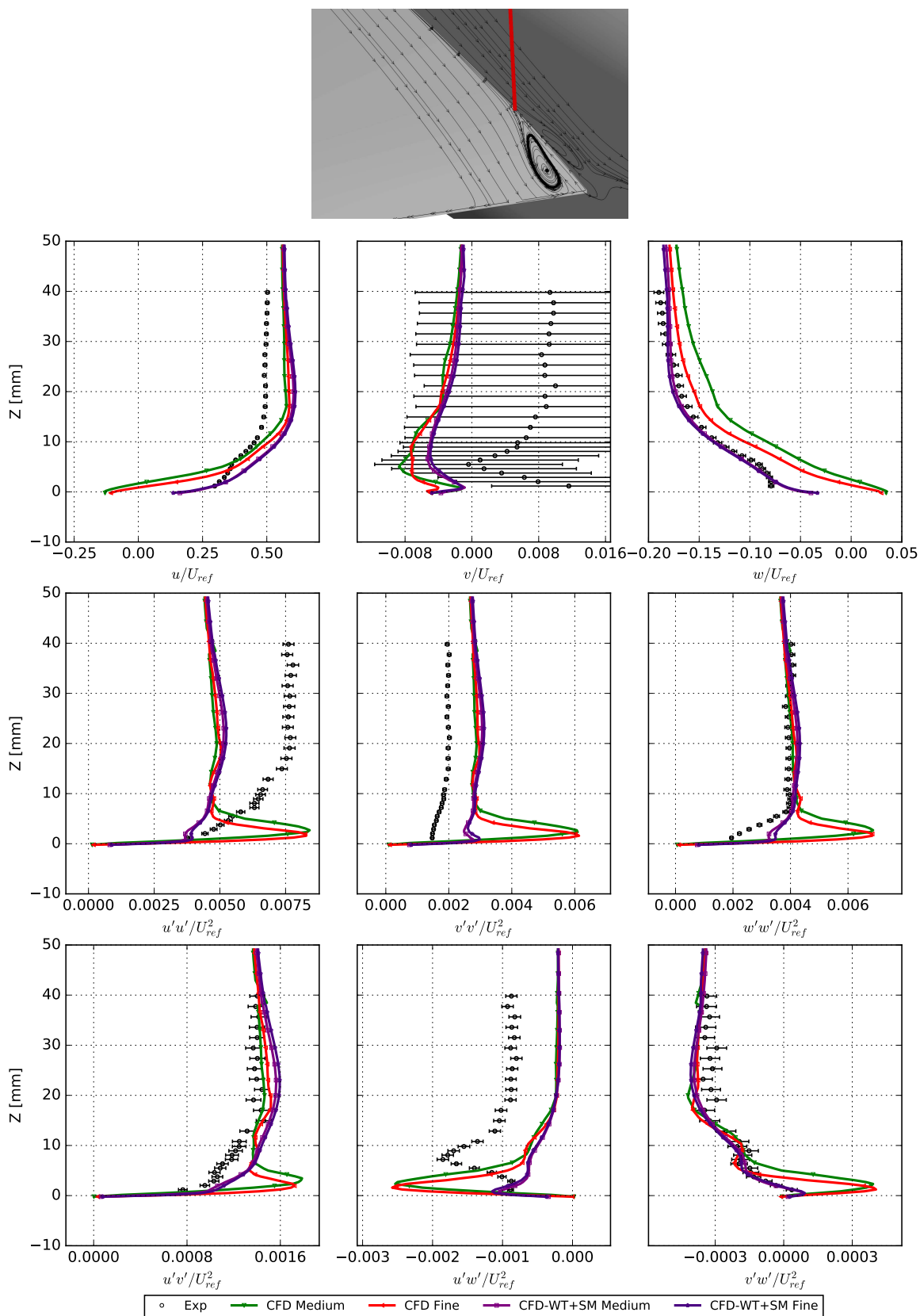


Figure 34. Tunnel Wall Effect Comparison Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2822.6$, $y = 237.1$, close to start of separation, 1 mm from fuselage.

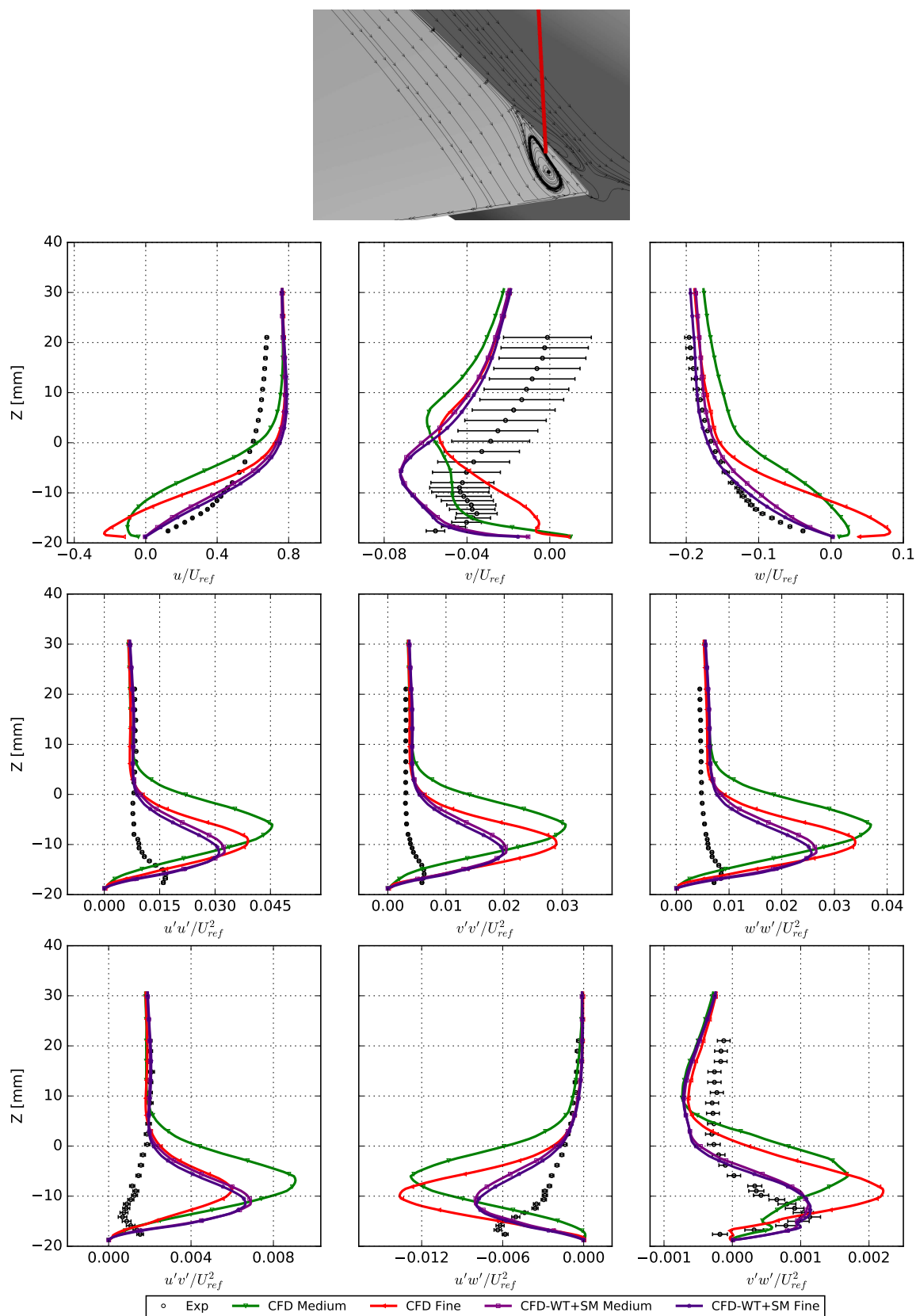


Figure 35. Tunnel Wall Effect Comparison Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2892.6$, $y = 246.1$, in the separation bubble.

C. CFD Turbulence Model Comparison

The effect of different turbulence models, including:

1. SA-Noft2-RC-QCR2013 (SARC-QCR)
2. SA-Noft2-RC (SARC)
3. SST-RC-QCR2013 (SSTRC-QCR)

on the juncture flow region, are explored in this section. While all the grid resolutions were run with the three turbulence models, results only on the fine grid at $\alpha = 5.0^\circ$ will be shown, for brevity. Additional results will be available on the Turbulence Modeling Resource website [25].

Figure 36 shows the separation bubble topology for the various turbulence models runs. Both SARC and SSTRC-QCR predict a larger bubble size than SARC-QCR.

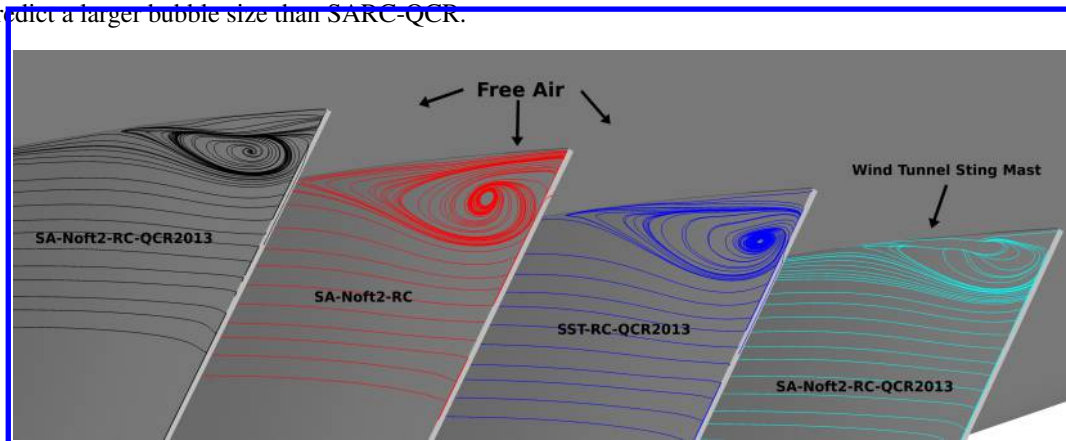


Figure 36. Side of body separation bubble topology vs turbulence model $\alpha = 5.0^\circ$.

Figure 37 shows the C_P slices at various stations. Overall, the pressures are very similar throughout most of the flow, with the largest differences occurring at the leading edge peaks, the separation zones, and the wing tips.

Comparisons between the velocity profiles and Reynolds stress profiles are shown in Figs. 38 through 43. It is hard to say which model performs best overall, as they all trade off. SSTRC-QCR seems to better match the experiment's Reynolds stresses, in Figs. 38 and 39, yet miss on the w component of velocity. SARC in the nose and leading edge region over-predicts some Reynolds stresses, and under-predicts others.

Near the trailing edge, in Figs. 40 and 41, SSTRC-QCR seems to have a different profile than the SA-based turbulence models. The SA models generally have a similar profile. However, at the start of the separation, Fig. 42, the SSTRC-QCR and SARC models have predicted separation, while the SARC-QCR model has not. From the earlier bubble size measurements, both the SSTRC-QCR and SARC models over-predicted the separation size across all the grids, and the profiles here show that as well. There is almost no correlation to the profiles in the separation bubble, in Fig. 43, between the turbulence models. Further examination of this data is needed, to fully understand how each turbulence model is affecting the juncture flow.

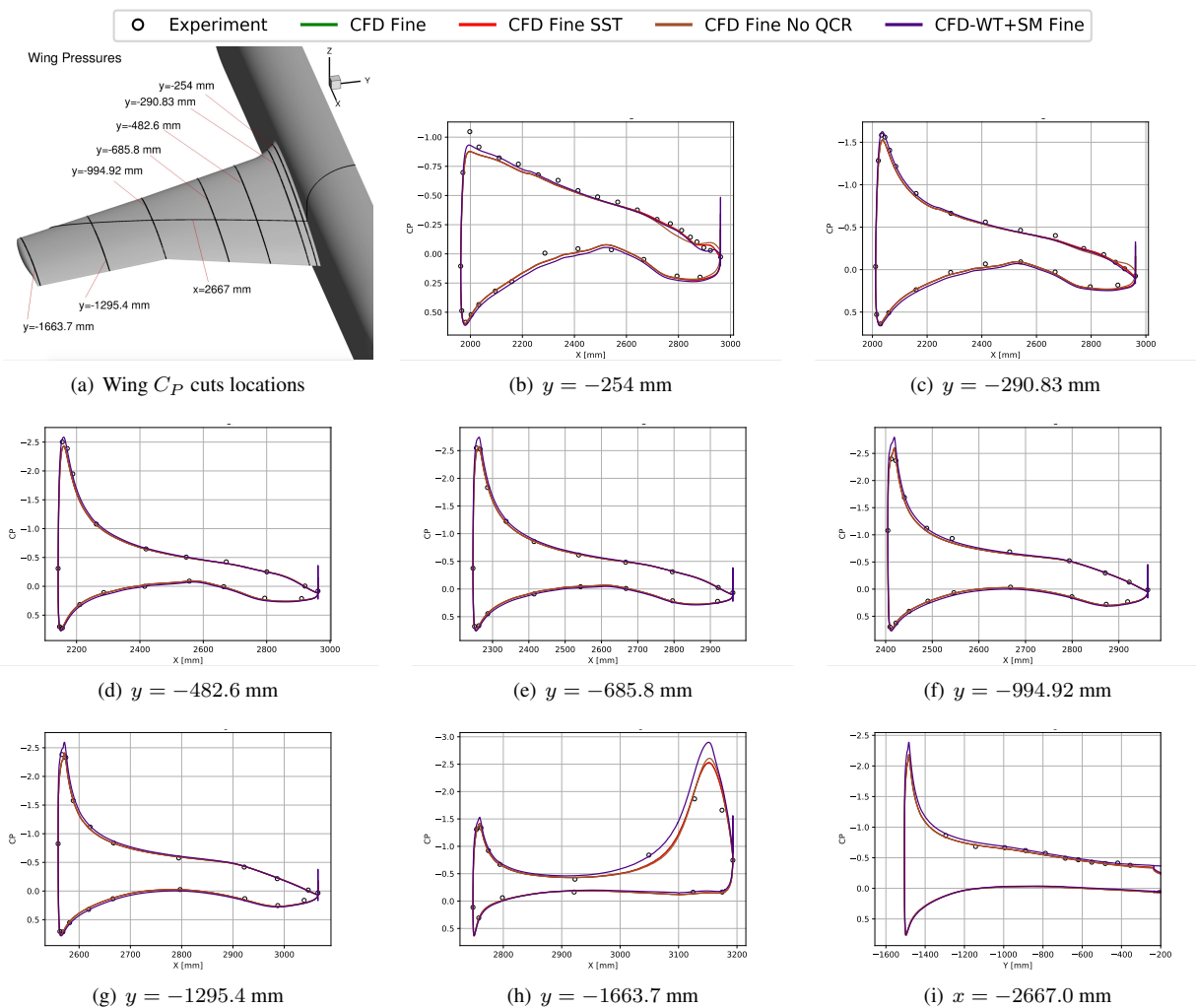


Figure 37. C_P slices for $\alpha = 5^\circ$ for the CFD Air Fine grid.

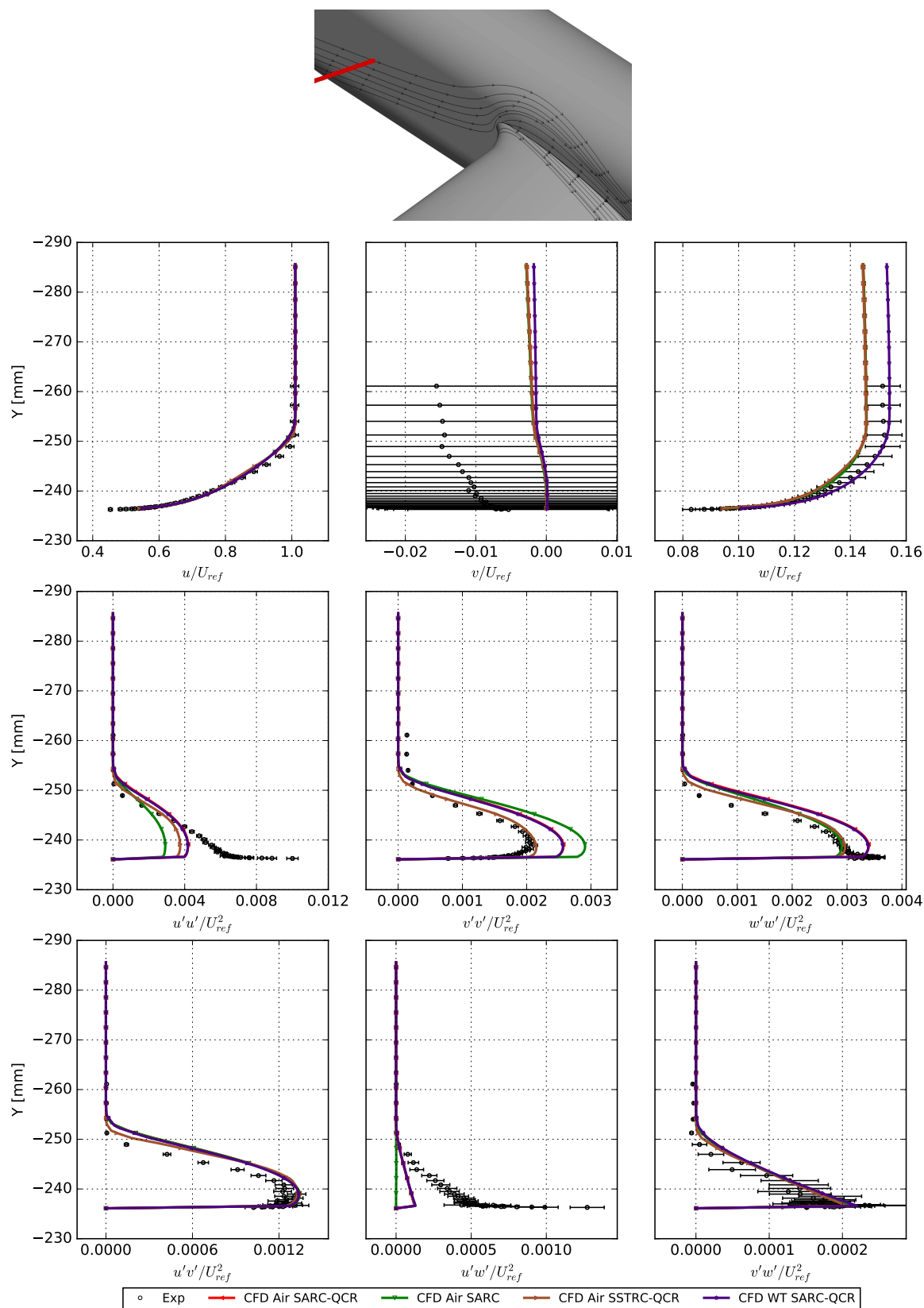


Figure 38. Turbulence Model Comparison: Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 1168.4$, $z = 0.0$, just past nose of fuselage.

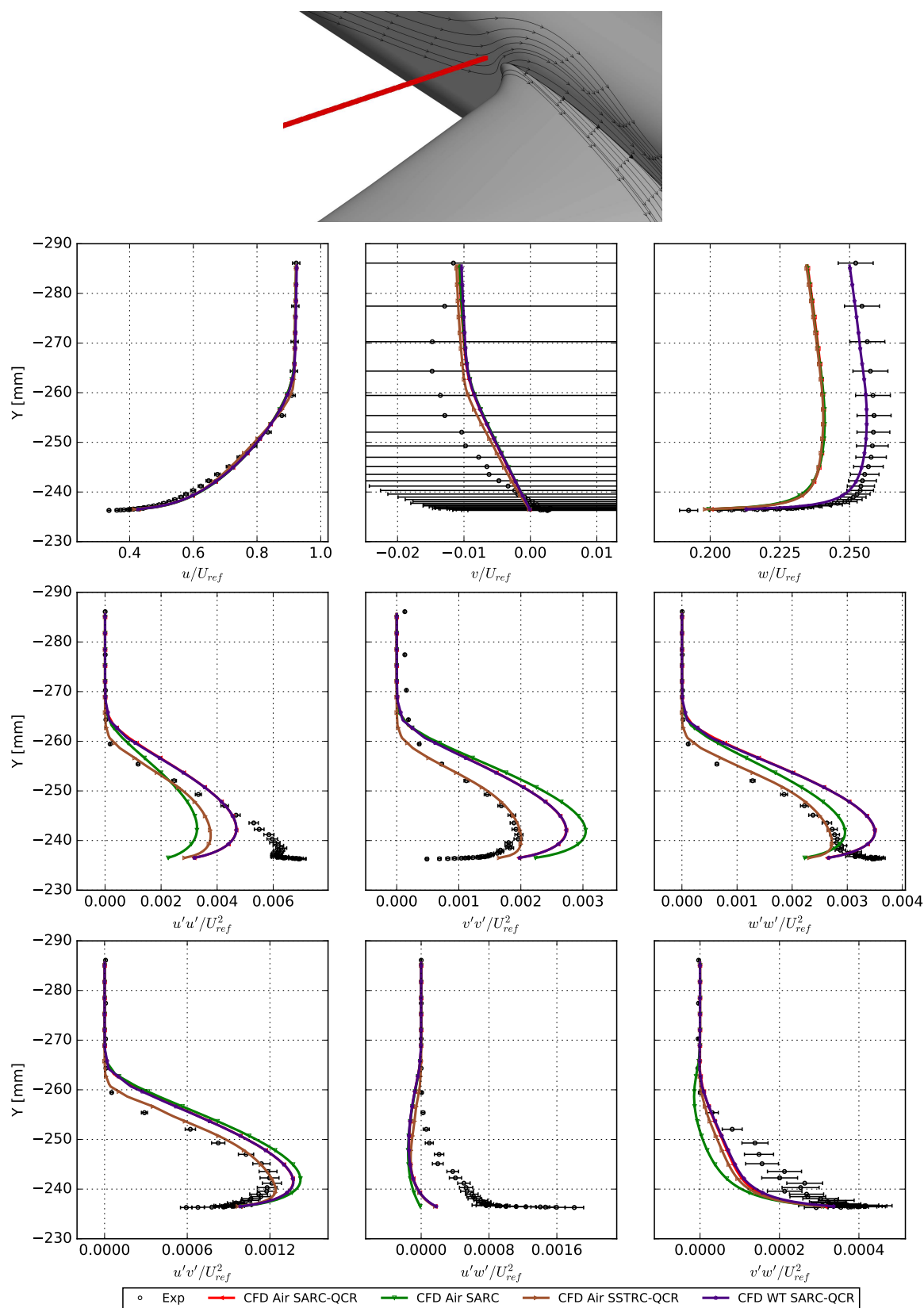


Figure 39. Turbulence Model Comparison: Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 1859.2$, $z = 55.05$, just upstream of LE.

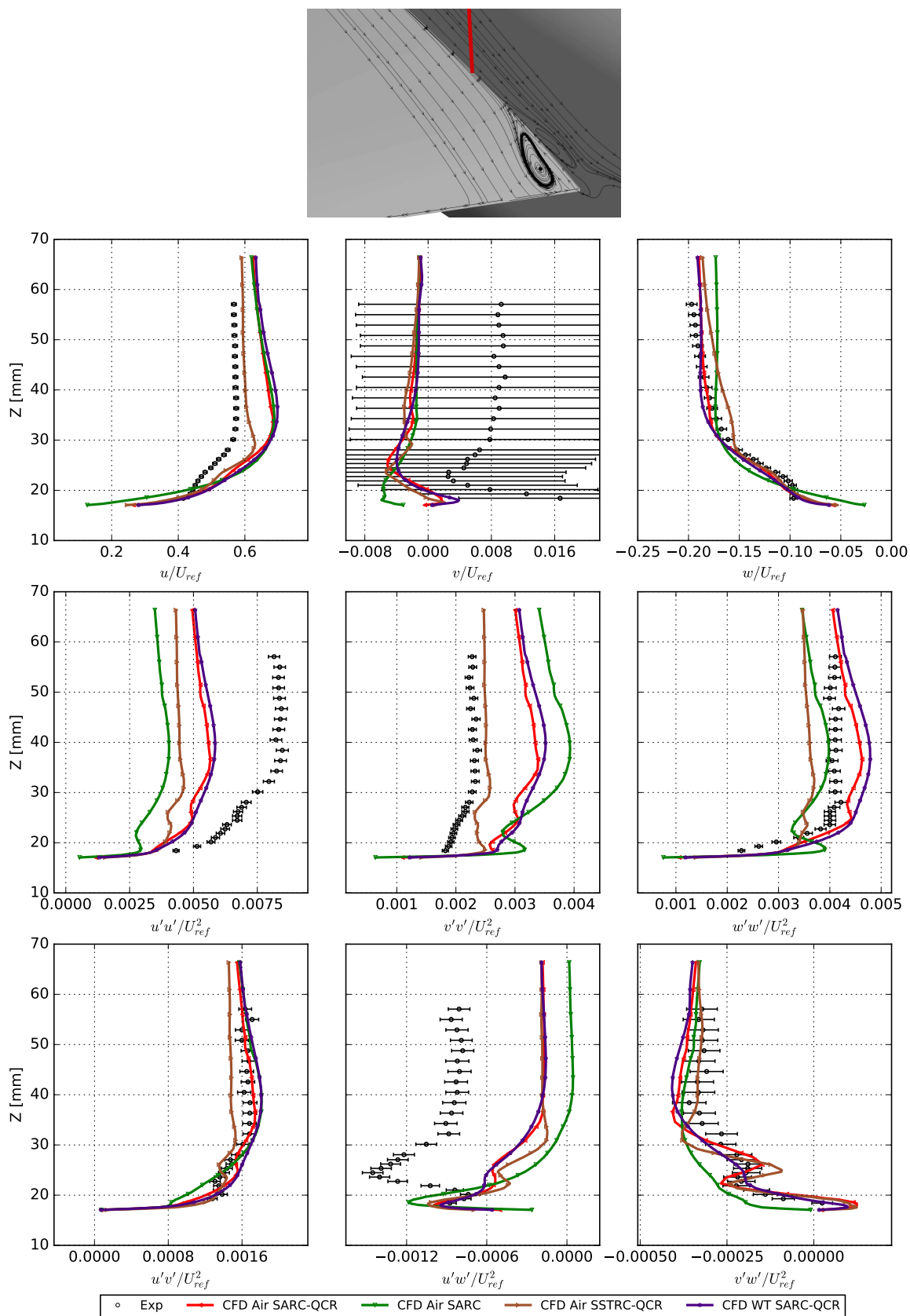


Figure 40. Turbulence Model Comparison: Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2747.6$, $y = 237.1$, upstream of separation, 1 mm from fuselage.

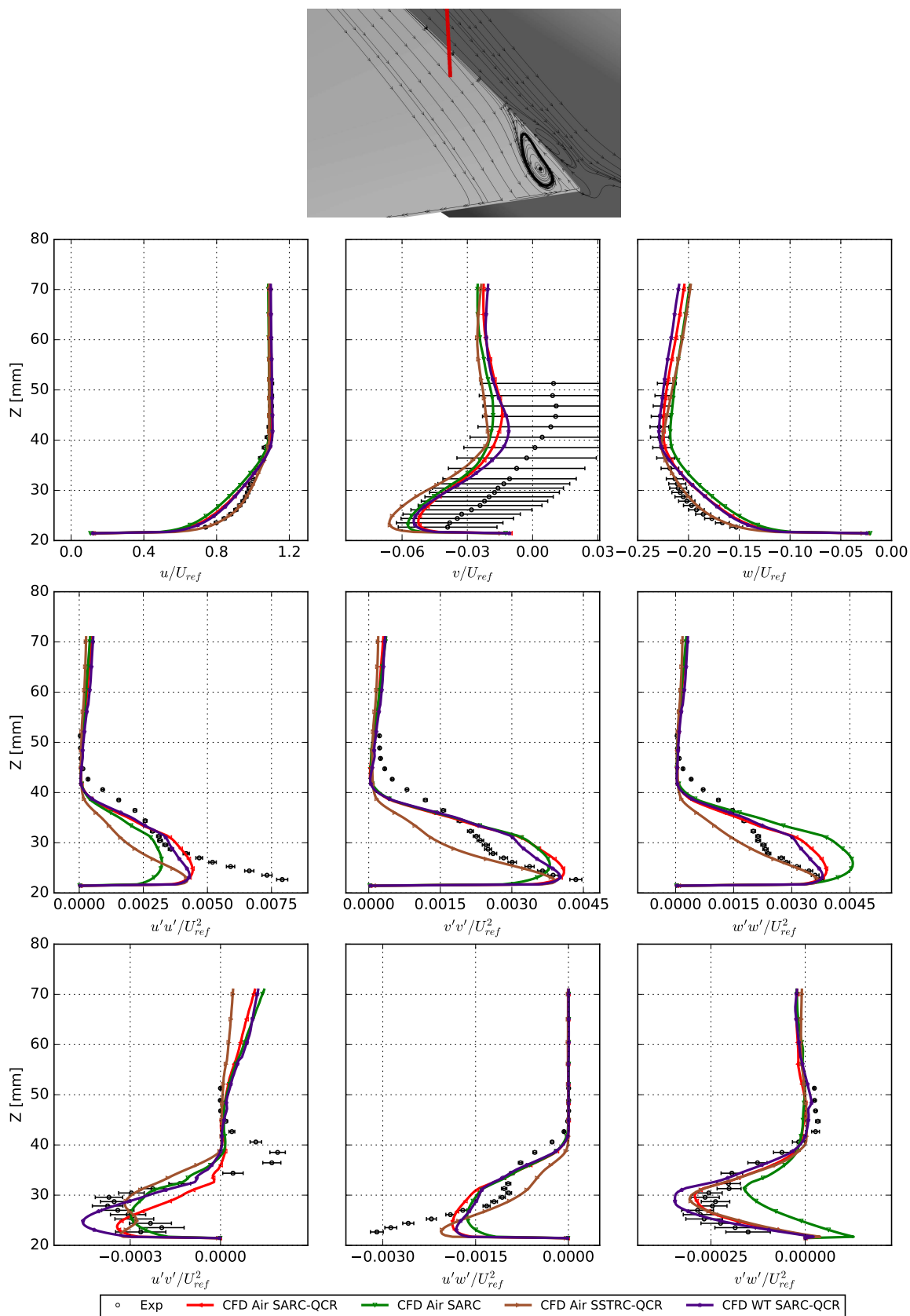


Figure 41. Turbulence Model Comparison: Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2747.6$, $y = 266.1$, upstream of separation, 30 mm from fuselage.

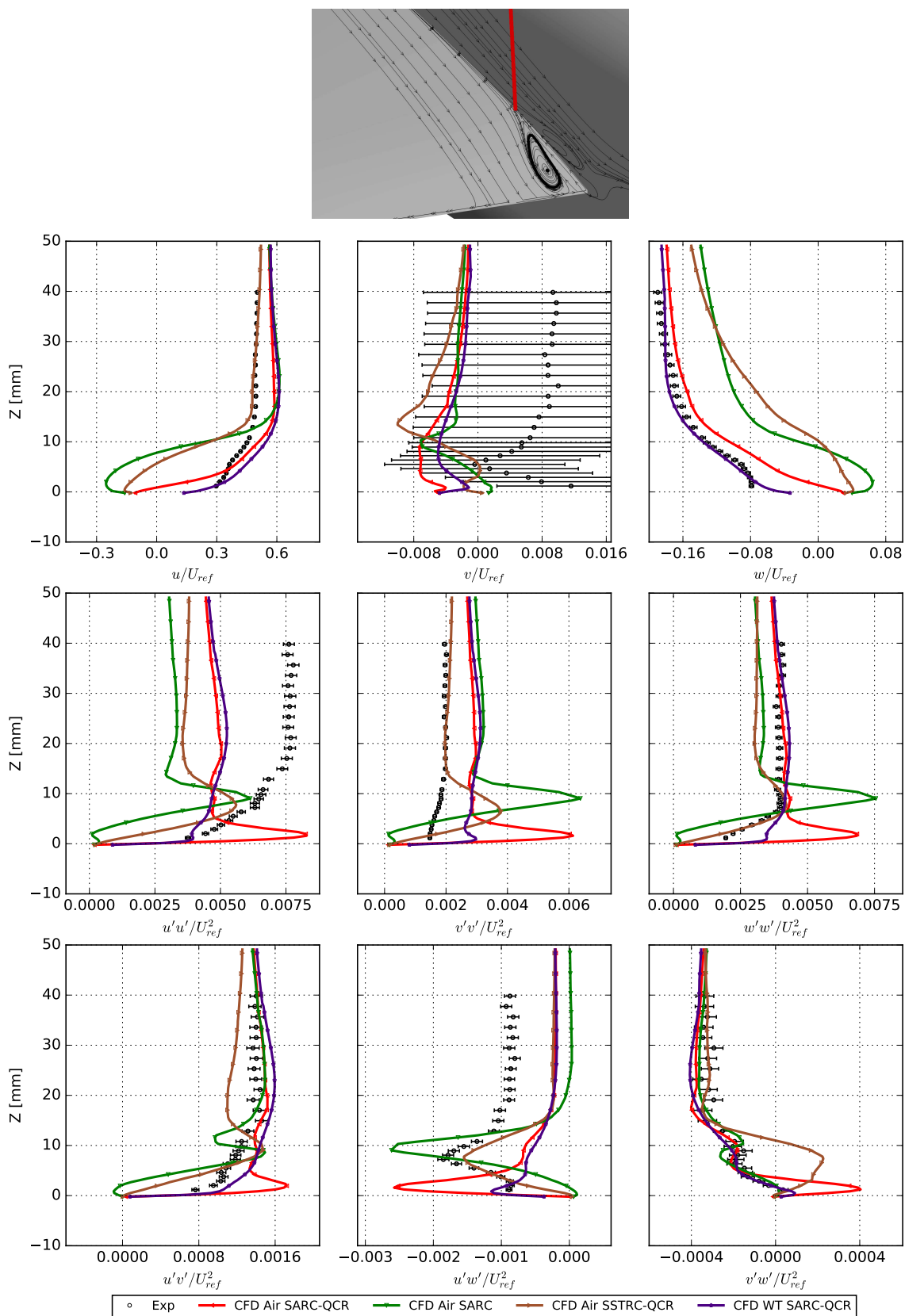


Figure 42. Turbulence Model Comparison: Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2822.6$, $y = 237.1$, close to start of separation, 1 mm from fuselage.

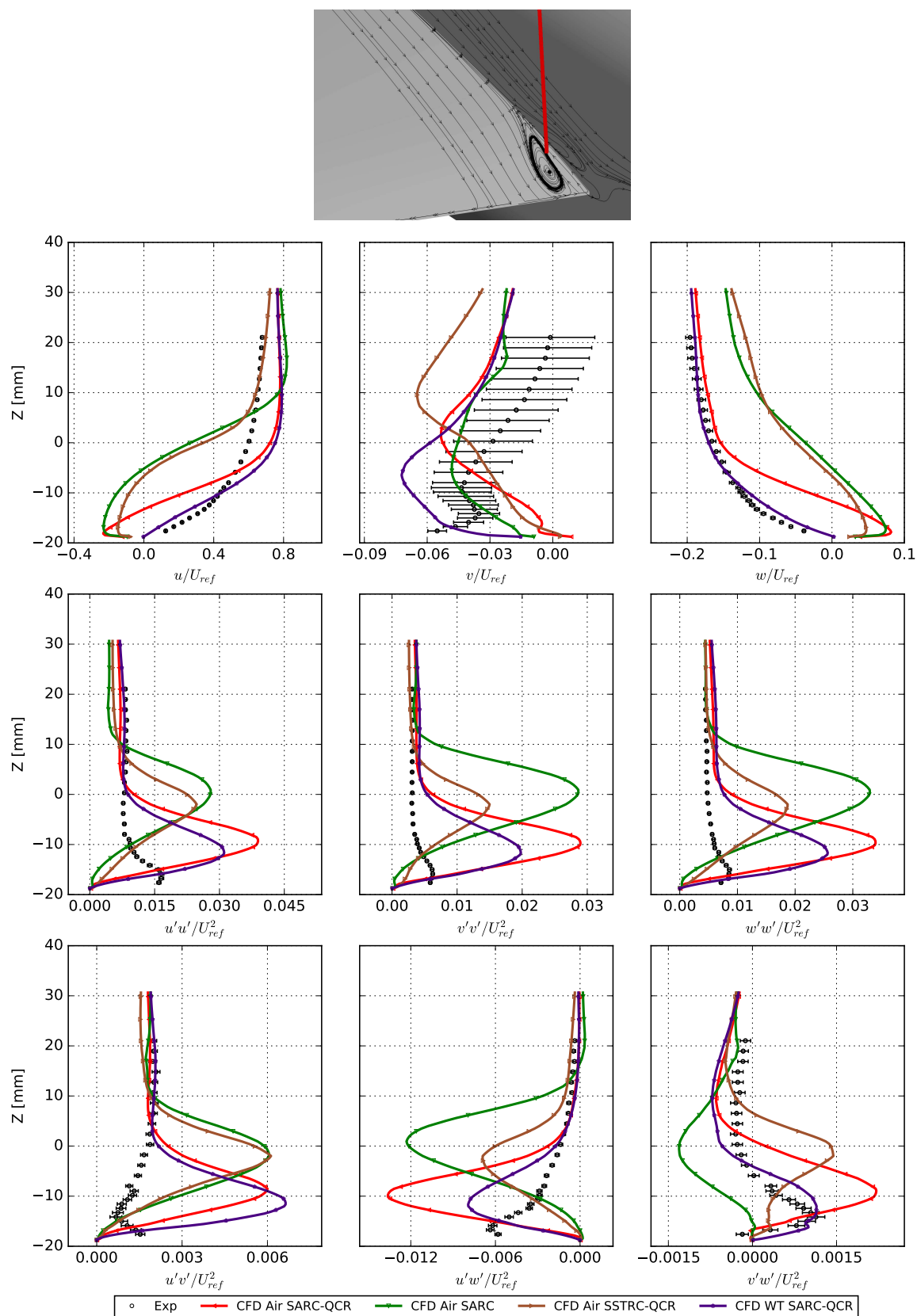


Figure 43. Turbulence Model Comparison: Velocities and Reynolds Stresses at $\alpha = 5.0^\circ$, $x = 2892.6$, $y = 246.1$, in the separation bubble.

V. Conclusions

A series of CFD cases were run with Overflow as a companion to the first phase of the Juncture Flow Model experiment. The recent experiment¹⁰ provides detailed flowfield data in the wing-body junction (corner) region near the wing trailing edge where separation occurs. Preliminary CFD data was compared with experimental data, exploring where the current state of RANS CFD simulations lies. Juncture flow sensitivity to grid resolution, turbulence model, and tunnel walls was presented.

The data presented in this paper provides a preliminary look at how well (or poorly) today's state-of-the-art RANS CFD simulations perform. No specific judgments or assessments of the results based on comparisons with the experimental data have been made. It is expected that there will be differences, sometimes small and other-times significant. The purpose of this overall project is to provide data for improvements of Reynolds averaged turbulence models, assessment and development of LES and higher order turbulence models, and also provide validation data.

Interested readers are referred to the experimental papers, Kegerise et al. [10], Jenkins et al. [26] and the companion paper, Rumsey et al. [11]. An extensive NASA report on the experiment is forthcoming and future test are being planned. The experimental configuration, conditions and computational data will be eventually available on the Turbulence Modeling Resource website [25].

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