

# Strategies for Running Junction Flow CFD in the Tunnel

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# Introduction

- The Juncture Flow (JF) model was tested in the NASA Langley 14- by 24-foot tunnel (14x22)
  - See NASA/TM-2019-220286, June 2019
- Running CFD in “free air” neglects the influence of the tunnel walls
- This set of slides provides some suggestions for possible ways to run CFD “in the tunnel”
- CAD files are available
  - for the 14x22 high-speed leg
    - simplified as-built shape, from laser scan
  - for the JF model, sting, and mast (at 5 deg and -2.5 deg. model incidence)
    - positioning obtained from laser scans
    - JF model is the as-designed shape
      - Discussion regarding differences between as-designed and as-built shapes is given on:  
[https://turbmodels.larc.nasa.gov/Other\\_exp\\_Data/JunctureFlow/junctureflow\\_geometry.html](https://turbmodels.larc.nasa.gov/Other_exp_Data/JunctureFlow/junctureflow_geometry.html)
    - mast/sting shapes are approximated

# Modeling Fidelity

- Various levels of modeling fidelity can be chosen:
  - Tunnel fidelity:
    - Include entire high-speed leg with contraction and diffuser, or (less accurately) only include a portion thereof
    - Model the tunnel walls as viscous, or (less accurately) as inviscid
      - Note: the incoming tunnel wall boundary layers were roughly 4 - 5 inches (100 - 125 mm) thick at 5 - 6 feet (1.5 - 1.8 m) behind the start of the test section for the JF test
  - Model fidelity:
    - Include JF model only
    - Include JF model and sting only
    - Include JF model, sting, and mast

# Typical CFD Strategy for Boundary Conditions (BCs)

- Desired nominal flow conditions (from median dynamic pressure (Q) running conditions during Test 640):
  - $M = 0.189$
  - $T = 288.84 \text{ K}$
  - $Re = 2.4 \text{ million}$  based on  $L = 557.17 \text{ mm}$

- Typical BCs for CFD:

- At inflow plane, set total temperature and total pressure consistent with desired flow conditions. E.g., for ideal gas:

$$\frac{T_t}{T_{ref}} = 1 + 0.2(0.189^2) \quad \frac{p_t}{p_{ref}} = \left( \frac{T_t}{T_{ref}} \right)^{3.5}$$

- Adjust back pressure at outflow plane to achieve desired flow conditions (iteratively, by “hand” or automatically)
    - See NASA/TM–2018–219812 for example of automated method
    - Pressure was measured in the diffuser in the JF experiment, and may be used to help guide back pressure settings in the CFD; however, it is more important to match the conditions inside the test section (in whatever computational way that can be achieved)

# Considerations

- Achieving “the desired flow conditions” can be difficult
  - With a model in the tunnel, where should the  $M=0.189$ ?
    - Sometimes CFD practitioners choose a location in the test section that is upstream of the model, away from walls and “far enough” away from the model
      - But this is NOT how the tunnel is run
  - In the tunnel, upstream probes are used to measure specific quantities
    - Calibration equations then determine the conditions that would occur in the empty tunnel at a specific reference point (center of the test section at  $x=5.41$  m); these are the reference conditions
- The tunnel inflow conditions are not strictly constant
  - For example, there is a known small pressure deficit over the center region of the tunnel of up to approx. 1 psf when the tunnel Q is around 60 psf (details provided elsewhere in “Slides Describing Measured Inflow Characteristics”)
- CFD can have difficulties if separation occurs in the diffuser near the outflow boundary
  - Possible strategies:
    - Add constant-area extension on the back of the diffuser (see AIAA-2017-4126 and AIAA-2019-0080)
    - Employ inviscid walls in the diffuser (see AIAA-2019-0080)
    - Shorten or eliminate the diffuser so that outflow occurs prior to separation

# Locations of Probes in 14x22

- Probes in the 14x22 used to determine running conditions are:
  - Total Pressure (Station 711):
    - $(x,y,z) = (-18.105, -7.010, -4.084)$  m (1.646 m away from the north wall)
  - Static Pressure (Station 758):
    - $(x,y,z) = (-3.658, -3.048, 0)$  m (355.60 mm away from the north wall)
  - Stagnation Temperature (Station 770):
    - $(x,y,z) = (-0.140, -3.234, -0.269)$  m (82.55 mm away from the north wall)
  - Dewpoint sensor orifice (Station 770):
    - $(x,y,z) = (-0.140, -3.317, -0.187)$  m (on the north wall)

# 14x22 Equations

- Equations used in 14x22 to determine conditions\*:

$$\Delta p|_{\text{indicated}} = (p_t|_{\text{Sta.711}} - p|_{\text{Sta.758}}) \text{ [lbf/ft}^2\text{]}$$

$$C' = \mathcal{F}(\Delta p|_{\text{indicated}})$$

$$\Delta p_{\infty} = C' K_{\text{pr}} \Delta p|_{\text{indicated}} \text{ [lbf/ft}^2\text{]} \quad K_{\text{pr}} = 0.998$$

$$p_{\text{adjusted}} = (p_t|_{\text{Sta.711}} - \Delta p_{\infty}) \text{ [lbf/ft}^2\text{]}$$

$$M_{\text{adjusted}} = \sqrt{5 \left( \frac{p_t|_{\text{Sta.711}}}{p_{\text{adjusted}}} \right)^{2/7} - 1}$$

$$Q_{\text{adjusted}} = \frac{1}{2} \gamma p_{\text{adjusted}} M_{\text{adjusted}}^2 \text{ [lbf/ft}^2\text{]}$$

$$\begin{aligned} C' &= 1.1381 + 0.00017194 \Delta p|_{\text{indicated}} + 0.0000050536 \Delta p|_{\text{indicated}}^2 & 0 \leq \Delta p|_{\text{indicated}} < 46 \\ C' &= 1.06032 + 0.00354687 \Delta p|_{\text{indicated}} - 0.000031557 \Delta p|_{\text{indicated}}^2 & 46 \leq \Delta p|_{\text{indicated}} < 52.5 \\ C' &= 1.1473 + 0.00023339 \Delta p|_{\text{indicated}} & \Delta p|_{\text{indicated}} \geq 52.5 \end{aligned}$$

Additional calibration equations are used to determine the tunnel velocity and Reynolds number (see NASA/TM-2014-218513)

\*Closed test section, boundary layer removal system off; see NASA/TM-2014-218513 and NASA Technical Report 20190018049, 2019.

# Additional CFD Strategy for JF

- The “In\_tunnel” CAD files are given in terms of the tunnel coordinate system
  - i.e., the tunnel is “horizontal” and the model is positioned at an angle of incidence
- When running the CFD simulation in the tunnel, it may be useful to shift and rotate the coordinate system to match what was used by the JF experimentalists:
  - $(x,y,z)=(0,0,0)$  at the fuselage nose
  - x axis aligned with fuselage, z up, y out the starboard wing
  - units in mm
  - tunnel appears to be at an angle of incidence with respect to this coordinate system
- In this way, extraction of the JF data will be easier, and the velocities and Reynolds stresses will already be in the correct coordinate system

The approximate rotations/translations (in order) to get the model (with nose at  $(0,0,0)$ , x axis along the body axis, z up, and y out the starboard side) into position in the wind tunnel (all units in mm) are:

- Incidence angle = 5 deg:
  - X-rotation = 0.02622944 deg
  - Z-rotation = -0.021198898 deg
  - Y-rotation = 5.00004783 deg
  - X-translation = 2873.098936
  - Y-translation = -6.155033
  - Z-translation = 217.321846
- Incidence angle = -2.5 deg:
  - X-rotation = 0.02323800 deg
  - Z-rotation = -0.02444117 deg
  - Y-rotation = -2.49995206 deg
  - X-translation = 2908.038625
  - Y-translation = -6.031538
  - Z-translation = -107.753423

Reverse the order to go from wind tunnel position to body-axis position