

Developing hierarchical augmentations via the "Learning and Inference assisted by Featurespace Engineering (LIFE)" framework

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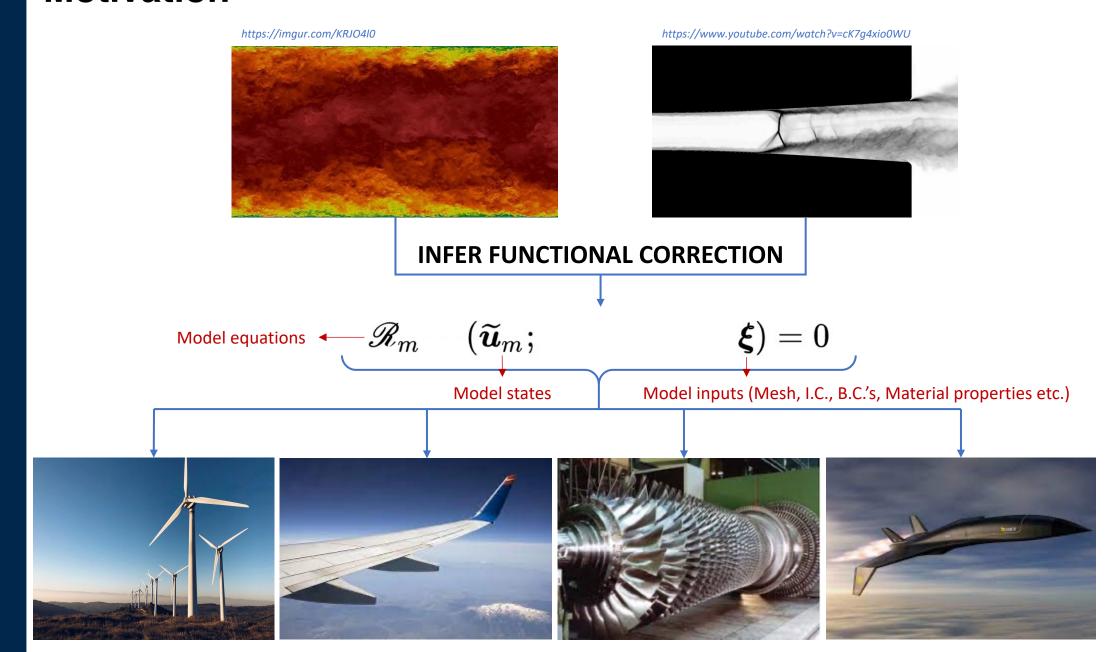
Background

LIFE

Hierarchical Augmentation

Summary

Motivation





Background – Integrated Inference and Machine Learning

Motivation

Background

LIFE

Hierarchical Augmentation

Summary

$$m{w}^* = rg\min_{m{w}} \sum_k \left(lpha_k \mathcal{C}^k(m{y}_{ ext{data}}^k, m{y}_{ ext{pred}}^k(m{ ilde{u}}_m^k; m{\xi}^k)) + rac{\lambda_k \mathcal{R}^k(m{ ilde{u}}_m^k, m{w}, m{\xi}^k)}{k}
ight)$$

s.t.
$$\mathscr{R}_{m,\mathrm{aug}}(\widetilde{m{u}}_m^k;eta(m{\eta}(\widetilde{m{u}}_m^k);m{w}),m{\xi}^k)=0$$



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Hierarchical Augmentation

Summary

Learning and Inference assisted by Feature-space Engineering

Where to augment?

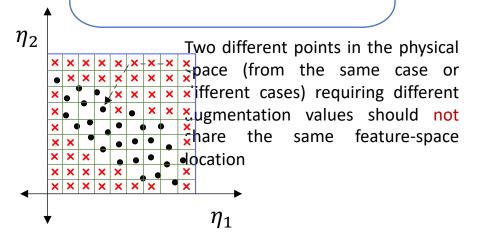
- ⇒ What is the intended correction?
- ⇒ How will the augmentation affect cases where correction is not required?
- ⇒ Physics-based limiting or regularization possible?

How to design feature-space?

- ⇒ Improve generalizability
- Features chosen by a modeler
- Non-dimensionalized using model quantities
- ⇒ Ensure predictive accuracy
- Enough features to roughly ensure a one-to-one features-to-augmentation map
- ⇒ Minimize extrapolation
- Bounded
- Parsimonious set of features

Which function class to use?

- ⇒ If available data populates the entire feature-space
- Neural Networks, Decision Trees
- Custom-built functions
- ⇒ Otherwise
- Localized learning





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Hierarchical Augmentation

Summary

Application: Bypass Transition

Adding an augmented bare-bones intermittency equation (inspired by Durbin's model of 2012) to Wilcox's 1988 k- ω model

$$\begin{split} \frac{D\rho k}{Dt} &= \boldsymbol{\nabla} \cdot ((\mu + \sigma_k \mu_t) \, \boldsymbol{\nabla} k) + \gamma \left(\mu_t \Omega^2 - \frac{2}{3} \rho k \frac{\partial u_i}{\partial x_j} \delta_{ij} \right) - C_{1k} \rho \omega k \\ \frac{D\rho \omega}{Dt} &= \boldsymbol{\nabla} \cdot ((\mu + \sigma_\omega \mu_t) \, \boldsymbol{\nabla} \omega) + C_{1\omega} \frac{\omega}{k} \left(\mu_t \Omega^2 - \frac{2}{3} \rho k \frac{\partial u_i}{\partial x_j} \delta_{ij} \right) - C_{2\omega} \rho \omega^2 \\ \frac{D\rho \gamma}{Dt} &= \boldsymbol{\nabla} \cdot ((\sigma_{\gamma,\ell} + \sigma_{\gamma,t} \mu_t) \, \boldsymbol{\nabla} \gamma) + \rho \Omega \left(\boldsymbol{\beta} - \gamma \right) \sqrt{\gamma} \end{split}$$

Replaced γ_{max} with augmentation and removed F_{ν} limiter

Intermittency transport equation smoothens augmentation field into intermittency field

Bounded augmentation: $0 \le \beta \le 1$ (as intermittency is driven by β)



Feature to help determine transition onset

$$Re_{\Omega} = rac{\Omega d^2}{2.188
u} \qquad \max_{d} Re_{\Omega} pprox Re_{ heta}$$

Physics-informed choice of features

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Summary

Praisner and Clark (J. Turbomachinery, 2007) gave the correlation

$$heta_{
m tr} pprox \sqrt{rac{7
u}{9\omega_{\infty}}}$$

Physics-based nondimensionalization

Then, we have
$$rac{Re_{ heta}}{Re_{ heta, ext{tr}}}pprox \max_{d}rac{Re_{\Omega}}{U_{\infty} heta_{ ext{tr}}/
u}pprox \max_{d}rac{\Omega d^2\sqrt{9\omega_{\infty}}}{U_{\infty}\sqrt{7
u}}$$

Freestream quantities are extracted from a constant wall distance.

Applying a conservative bound

$$\eta_1 = \min\left(rac{d^2\Omega\sqrt{9\omega_\infty}}{U_\infty\sqrt{7
u}},3
ight)$$

Bounded features



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Feature(s) to identify laminar/turbulent regions

Compare ν and ν_t . What about the viscous sublayer, though?

Compare d and ℓ_t to see if d is significantly larger. For k- ω model, $\mathcal{O}(\ell_t) = \mathcal{O}(\sqrt{k}/\omega)$

Mathematically bound both the features as:

$$\eta_2 = rac{d}{d+\sqrt{k}/\omega}$$

$$\eta_3 = rac{
u}{
u_t +
u}$$

- Too many features over-specify physical conditions and reduce generalizability
- Too few features can result in lower predictive accuracy even for the training cases



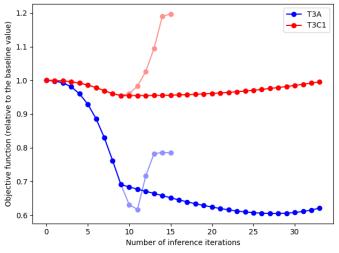
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Hierarchical Augmentation

Summary

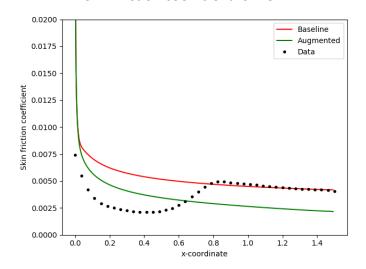
What happens when off-the-shelf NNs are used?



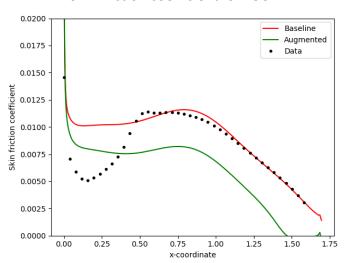
$$\mathcal{C}^k = rac{1}{N^k} \sum_i^{N^k} \left(C_f^k(x_i) - C_{f, ext{data}}^k(x_i)
ight)^2$$

Relative cost reduction w.r.t. inference iterations

Skin friction coefficient for T3A



Skin friction coefficient for T3C1





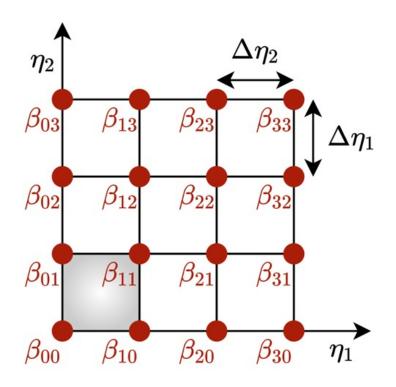
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Limited data necessitates localized learning



- C⁰-continuous
- Susceptible to curse of dimensionality
- Choice of grid resolution is crucial

For a feature space location in the shaded region, the multilinear expression reads

$$eta = eta_{00} + (eta_{10} - eta_{00})\eta_1 + (eta_{01} - eta_{00})\eta_2 + \cdots \ (eta_{11} + eta_{00} - eta_{10} - eta_{01})\eta_1\eta_2$$



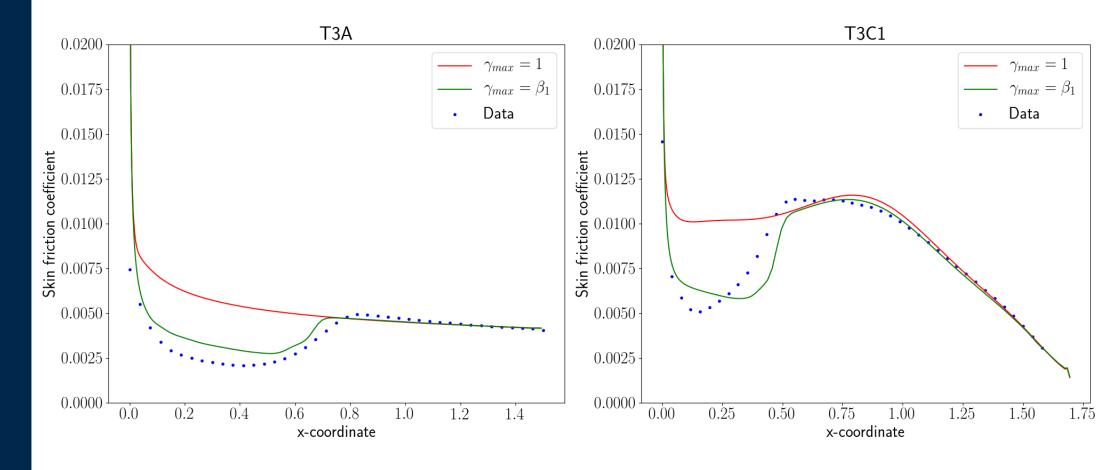
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Summary

A C⁰-continuous augmentation (Training)



- Feature-space uniformly discretized into 45x15x15 cells
- Excellent solver convergence compared to a discontinuous functional form for the augmentation
- Cost function was the sum squared discrepancy in the C_f profile



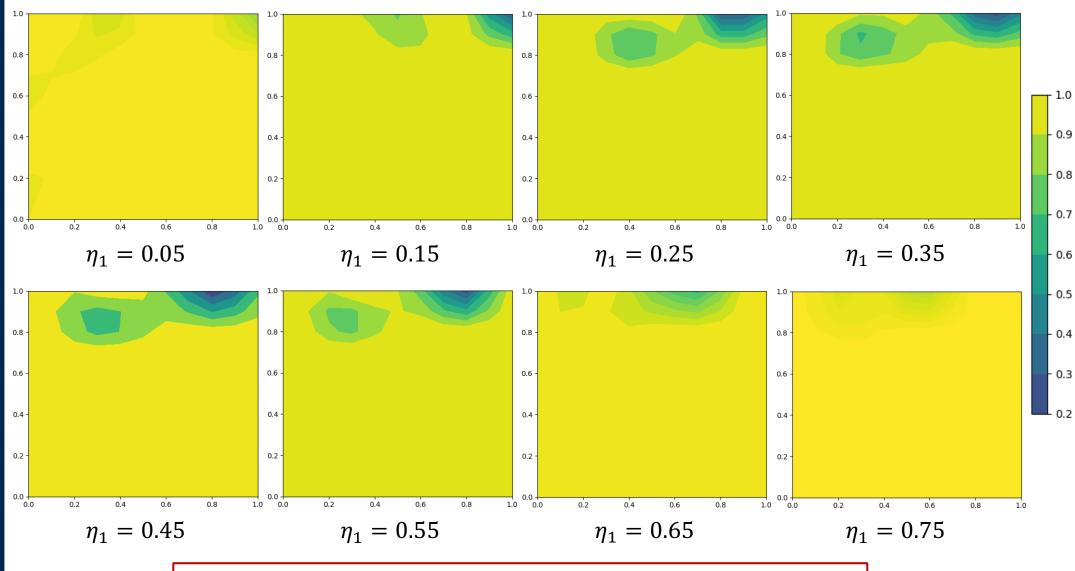
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How does the feature-space look?



For all plots:

X-axes: η_2 (0 to 1)

Y-axes: η_3 (0 to 1)



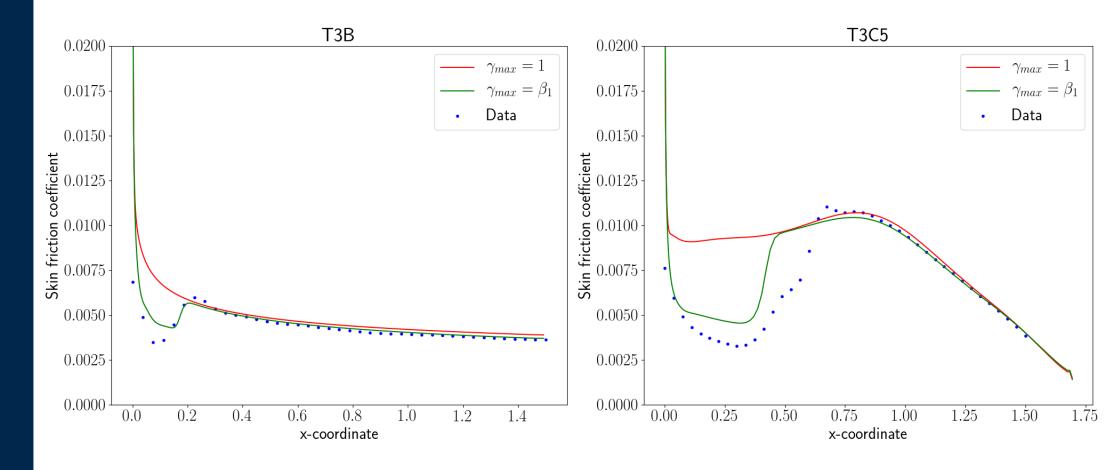
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A C⁰-continuous augmentation (Testing – FPG)



Good generalizability to zero and favorable pressure gradient cases



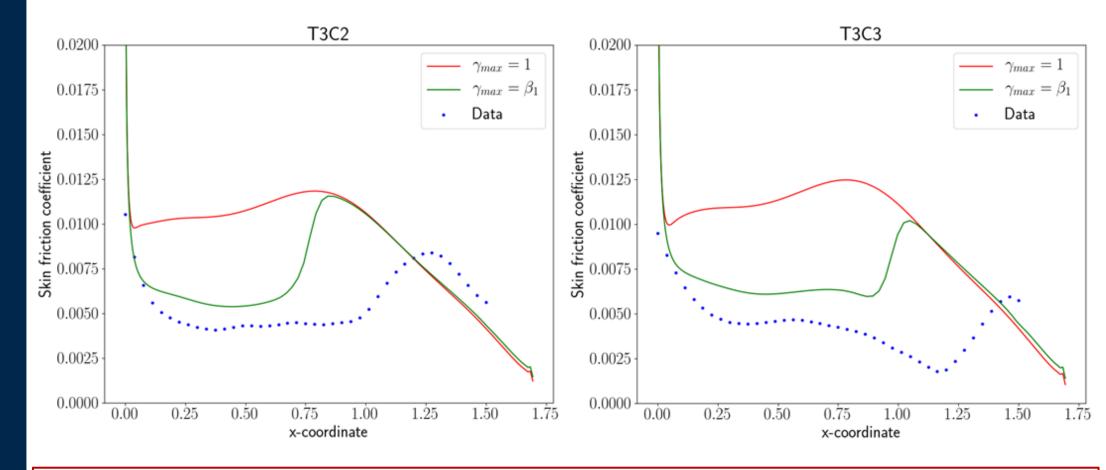
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A C⁰-continuous augmentation (Testing – APG)



Worse predictions for cases involving transition in adverse pressure gradient regions



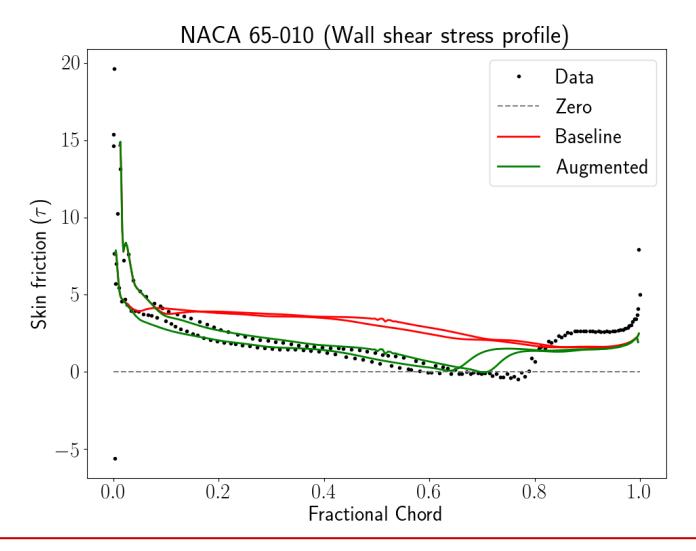
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Prediction on a compressor cascade (LES from RTRC)



- Transition predicted near separation location
- Downstream discrepancy results from inadequacy in underlying turbulence model



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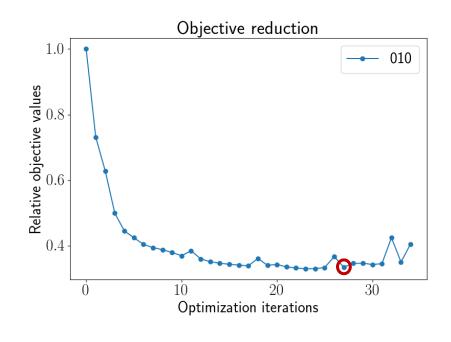
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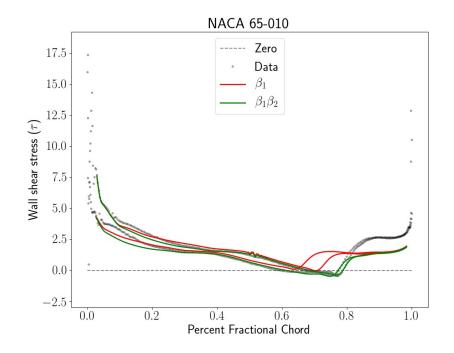
Hierarchical Augmentation

Summary

Inferring a Hierarchical Augmentation

$$rac{D
ho\gamma}{Dt} = oldsymbol{
abla} \left(\left(\sigma_{\gamma,l} \mu + \sigma_{\gamma,t} \mu_t
ight) oldsymbol{
abla} \gamma
ight) +
ho\Omega(oldsymbol{eta_1}eta_2 - \gamma)\sqrt{\gamma}$$





- Feature space uniformly discretized into $30 \times 10 \times 10$ cells for hierarchical augmentation
- Cost function was the sum squared discrepancy in the wall shear stress profile
- Using the hierarchical augmentation as is results in poor predictions on the flat plate cases



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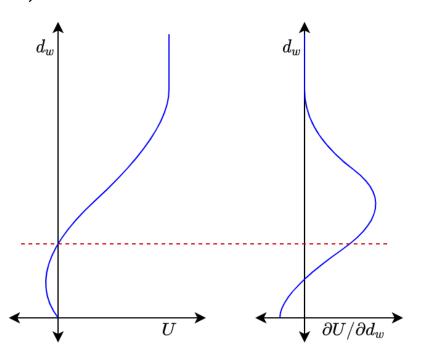
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Designing a physics-informed blending function

$$rac{D
ho\gamma}{Dt} = oldsymbol{
abla} \left(\left(\sigma_{\gamma,l} \mu + \sigma_{\gamma,t} \mu_t
ight) oldsymbol{
abla} \gamma
ight) +
ho (eta_1 eta_2^{oldsymbol{\sigma}} - \gamma) \sqrt{\gamma} \Omega_1^{oldsymbol{\sigma}}$$

$$\sigma = rac{1}{1+\expigg(-rac{f_{\sigma}+0.05}{0.003}igg)}$$

$$\sigma = rac{1}{1 + \exp\left(-rac{f_{\sigma} + 0.05}{0.003}
ight)} \hspace{0.5cm} f_{\sigma} = \left(rac{\sqrt{
u/\Omega}(oldsymbol{n}_w\cdotoldsymbol{
abla})\Omega}{\sqrt{
u/\Omega}|(oldsymbol{n}_w\cdotoldsymbol{
abla})\Omega| + \Omega}
ight) \left(rac{\omega}{\sqrt{2}\Omega + \omega}
ight) .$$





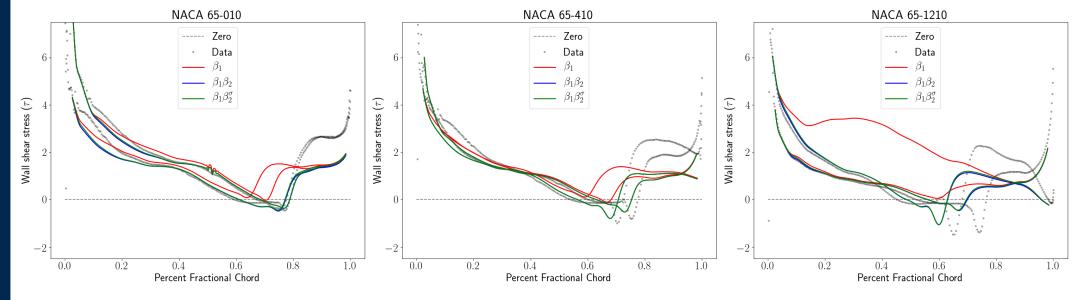
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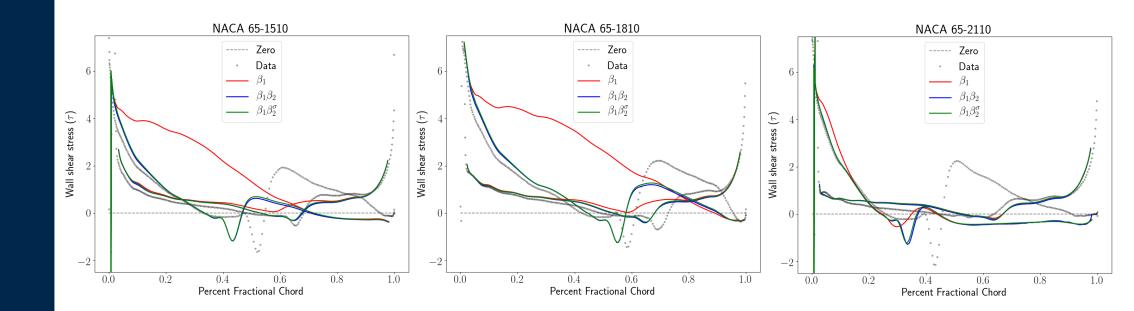
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Predictions using the hierarchical augmentation







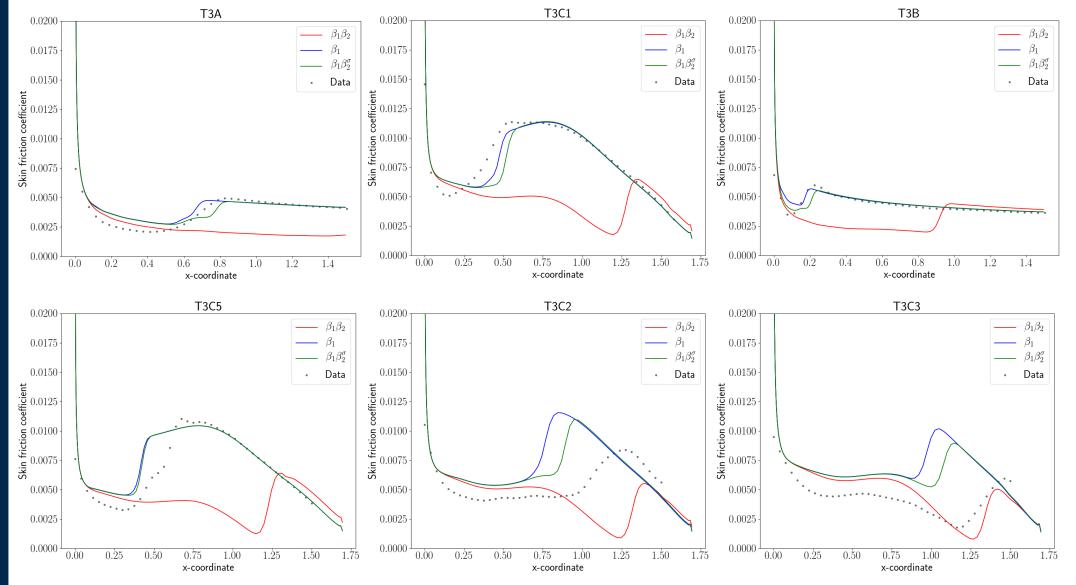
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Hierarchical Augmentation

Summary

Predictions using the blended hierarchical augmentation



Blending function affects (and slightly improves) predictions for transition in APG regions



Background

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Hierarchical Augmentation

Summary

Summary

- A C⁰-continuous augmentation function provides excellent solver convergence and added implicit regularization
- The LIFE framework was used to infer two augmentations:
 - β_1 inferred from *two flat plate cases*
 - Training cases involved transition of attached flows in zero/favorable pressure gradients
 - Transition predictions generalize to unseen zero/favorable pressure gradient configurations well
 - Transition is predicted significantly upstream in adverse pressure gradient regions
 - β_2 subsequently inferred from <u>one compressor cascade case</u>
 - Training case involves separation-induced transition
 - Transition location predictions significantly improve across all test configurations
 - Transition is predicted slightly upstream compared to what is observed from the LES data in some instances
- An appropriate blending function (σ) was designed to shield attached flow regions from the effects of the second (hierarchical) augmentation
- Future work will include exploring purely local feature candidates and the blending function in addition to building a formal framework to optimize hyperparameters for localized learning